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USATSARCOM TECHNICAL REPORT 83-1

APPROVED FOR PUBLIC RELEASE DISTRIBUTION UNLIMITED

HISTORICAL INFLATION PROGRAM

(A COMPUTER PROGRAM GENERATING HISTORICAL INFLATION INDICES FOR ARMY AIRCRAFT)

WARREN H. GILLE, JR. JAMES R. HAMILTON

FINAL REPORT MARCH 1983

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U.S. ARMY TROOP SUPPORT AND AVIATION MATERIEL **READINESS COMMAND COMPTROLLER** COST ANALYSIS DIVISION 4300 GOODFELLOW BLVD. ST. LOUIS, MISSOURI 63120



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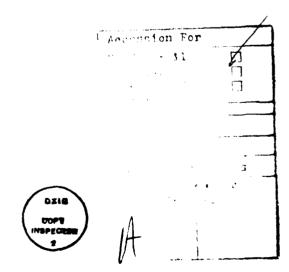
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20. ABSTRACT.

These indices and factors provide a means of adjusting historical cost data for the procurement of Army aircraft to constant year dollars. Additional features include: computations for the derivation of revised weighting factors, detailed indices enabling the adjustment of historical labor and material costs separately, a discussion of aggregate weighting factors for labor and materials (including trends from sensitivity analysis with more background materials), and additional documentation aimed at making the report useful to a large cross section of the DOD rotary wing aircraft community. This report has been revised to include the latest information concerning the UH-60A BLACK HAWK. This system has been integrated into the Historical Inflation Program for Army aircraft.



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ACKNOWLEDGEMENTS

The authors extend their appreciation to the Kansas City Regional Office of the Bureau of Labor Statistics, U.S. Department of Labor, for special assistance with wage and price data.

Credit is due Mr. John M. Barnett and Mr. H. Kevin Wille for supplying research material and data from their paper entitled <u>UH-60A BLACK HAWK</u> Aircraft System Peculiar Historical Inflation Indices.

Appreciation is extended to Mr. Bruce Powell, USATSARCOM DMIS, who provided the programming assistance required to introduce the UH-60A High-Technology aircraft into the Historical Inflation Program.

Mrs. Marva Campbell provided excellent clerical support in the revision of this paper.

DISCLAIMER STATEMENT

The views, opinions, and/or findings contained in this report are those of the author(s) and should not be construed as an official Department of the Army position, policy, or decision unless so designated by other documentation.

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I. <u>APPLICABILITY</u>. The inflation indices and factors published in this report are applicable to the adjustment of historical costs for the procurement of Army aircraft. These costs are currently funded by the Aircraft Procurement, Army and Other Procurement, Army appropriations.

II. AN OVERVIEW OF THE HISTORICAL INFLATION PROGRAM

A. History

The Historical Inflation Program for Army aircraft procurement was developed using a series of documents, the first being Aerospace Price Indices, by H.G. Campbell, (December 1970).

This document established a basis for the construction of general aircraft indices, identified items of special interest and concern, and demonstrated the importance of thorough analysis of material composition when constructing an historical index. Between 1973-1976, the United States Army Aviation Systems Command (USAAVSCOM) developed several indices for rotary wing aircraft, and since 1977 this function has been performed by the Components and Operational Studies Branch, Cost Analysis Division, Office of the Comptroller, USATSARCOM.

The current indices are based on research done in the period 1972 to date. In July 1973, the Office of the Comptroller, Cost Analysis Division, made a study of materials used in the Army helicopter systems then, or most recently, in production. Cost Information Reports were assembled, and contractors were asked to supply lists of materials for both airframe and engine, on the basis of contribution to weight. Contractor technical and engineering personnel provided assistance with data interpretation and definitions for items whose composition was unclear from engineering documents and Detailed Weight Statements. In January 1983, a special research study entitled UH-60A BTACK HAWK Aircraft System Peculiar Inflation Indices was written by

H. Kevin Wille and John M. Barnett (ref 9) and data from this study has been included in this report.

The following aircraft have been selected:

UH-1 OH-6 AH-1 UH-60A CH-47 OH-58 CH-54

This selection of aircraft is deemed typical for several reasons. First, the seven helicopter systems listed above make up over 90% of the U.S. Army's current helicopter fleet. Second, a number of these aircraft have been produced on a long term, continuous basis in numerous models. Third, they are among the systems most likely to be used in developing Cost Estimating Relationships for new systems by use of parametric techniques. And fourth, they include the new high technology UH-60A BLACK HAWK aircraft.

The September 1973 historical inflation cost research report, cited in the references, was the first report to make use of this type of information. It was updated by the August 1974 cost research report, and then by a series of expanded analyses under current title, <u>Historical Inflation Program</u>, since that time. A list of the assumptions and changes in methodology over the period referenced are included in the technical section of this report.

B. Construction of Indices - Methodology.

The indices are developed by a stepwise, building process, which computes the contributions to cost on a weighted, value-added basis.

- 1. First, the contribution to cost of small parts and other purchased equipment is calculated.
- 2. Next, the cost contribution of purchased parts is combined with that of raw materials to get the cost of purchased materials.
- 3. Cost of purchased materials is then combined with contractor labor cost to compute the index for components such as engine or airframe.
- 4. The indices for engine, airframe, and avionics are combined to get indices for aggregate aircraft.

C. Indexing Techniques.

The procedure used is "cost-weighting". The information obtained from the 1973 research entitled Material Composition of U.S. Army Helicopters established percentages based on weight. Because the indices used to track material costs are based on monetary considerations (e.g., Producer Price Index; Wages, by Standard Industrial Code), percentages by weight had to be transformed into percentage contributions to cost, if PPI and SIC inflation factors were to be applied directly. Based on the premise of profit maximization, contractors should tend to minimize the use of expensive materials subject to maintaining acceptable performance standards; essentially, materials with a high cost per unit weight ratio would be used sparingly. Adjusting a percentage based on weight using a monetary index would not only result in an improper index initially, but also one with diminishing reliability. The latter bias is avoided by calculating

the contribution to cost, instead of merely the contribution to weight.

- D. Weighting Factors. Although the model is developed by an iterative, stepwise process, the revised weighting factors in the table at the end of Appendix B implicitly include all calculations. The index, as stated, is merely the direct sum of the products of the weights and their corresponding material index values. The development of weighting factors is illustrated in the Technical Section.
- E. <u>Data</u>. The data used in the program are inputted in two different forms. Yearly data are presented by calendar year 1947 to date, and monthly data are presented for 1967 to date. The yearly data, pre 1958, are condensed into three columns; the data for 1958 and later are presented in an 18 column format (14 columns for material and 4 for labor). The data, their characterization, and any redefinition by the Bureau of Labor Statistics over the years, are tracked in line diagram C-2.

F. Validity and Firmness of Data.

The Producer Price Index and hourly wage data were supplied by the Kansas City Regional Office of the Bureau of Labor Statistics, U.S. Department of Labor. The data comes in three types of published format: (1) a cumulative history covering past years on a monthly basis,

(2) an annual publication (such as the <u>Producer Prices and Price Index Annual Supplement</u>) which lists the previous 12 months, and (3) monthly publications which list the most current month and several other months for comparison.

For data to be "firm" it must be at least 18 months old because it is benchmarked and adjusted after the fact. Only small samples are taken throughout the year. However, during one month, the benchmark month, a much more comprehensive sample is taken. Due to its significantly larger sample size, the benchmark month sample is felt to be more representative than those of other individual months. If the benchmark value diverges significantly from the pattern, the other months are adjusted proportionately to conform to its base as benchmark.

The data in a cumulative history publication is felt to be firm or "final". Basically, such publications provide a chronological listing of all firm data available for the past history of those indices. However, the data in these publications is usually 18 to 24 months behind the current period. The data for each month listed in the annual supplements is not necessarily firm because benchmarks occur during the calendar year, and at different times for different series. Adjustments may not have been made before the annual supplements are published. The data in the monthly publications are even less firm. In general, the Producer Price Index data are firm before the wage indices for the corresponding month, due to the fact that it is easier to define and measure price changes for commodities than for human skills.

G. Respecification of the Data Set

From time to time, the Bureau of Labor Statistics redefines labor and material codes to meet the changing needs of its clientele and to cope with a variety of sampling problems. Due to respecification or deletion of PPI codes by BLS, the data set used in the Historical Inflation Program must change. The changes since the last report are as follows:

OLD CODE AND TITLE	NEW CODE AND TITLE
10130262 Sheets, C.R. Carbon	10170711 Sheets, C.R. Carbon
10150153 Alloy Steel Forgings	10151351 Closed Die Forgings
10220111 Lead, Pig	10220127 Lead, Pig
1025013 Rod, Screw, Stock	10250141 Rod.Screw.Stock

The historical flow of the labor and material data from 1947 to date is illustrated by chart C-2, in appendix C.

H. Introduction of the UH-60A BLACK HAWK Aircraft

In October 1978, the first UH-60A Black Hawk helicopter was delivered to the U.S. Army. With development of the Black Hawk, an era of high technology was introduced into the construction of Army aircraft. The airframe and T700 engine of the Black Hawk embody significant technological improvements as compared with previous Army aircraft. Beginning in 1980, preparations to include the UH-60A Black Hawk in the <u>Historical Inflation Program</u> for Army aircraft were undertaken.

The addition of Black Hawk to the <u>Historical Inflation Program</u> required a reevaluation of the Army's average helicopter. With

the inclusion of the Black Hawk, it was evident that the weights accorded high-tech materials such as titanium and monel metal would increase. However in 1980 it was not known how Black Hawk would affect the average bill of materials in the <u>Historical</u>
Inflation Program or the indices themselves.

The first attempt to study the content of Black Hawk within the perspective of historical inflation was by H. Kevin Wille and John M. Barnett in their paper <u>UH-60A Black Hawk Aircraft System</u>

Peculiar Historical Inflation Indices (reference 9). The same material data and resources were used to construct their system peculiar indices were used to revise the <u>Historical Inflation</u>

Program. The most important conclusion reached concerning the calculation of inflation indices in the revised aircraft paper was that the 14 material and 4 labor categories previously established could be retained.

The second conclusion, of course, was that the relative weights of the combined bill of materials had changed and that the contributions to cost of each cost component would have to be recalculated. This was done using ratio and proportion techniques on the original analysis to establish the revised, hi-tech index equations.

The indices exhibit significant change, especially in the engine index. In addition to the current FY 82 index, the hi-tech index is also now used for FY 80 and FY 81. The reasons for this are two. First, between 1978 and 1980 the pipeline for Black Hawk was filled. Second, according to the TSARCOM project managers, in 1980, Black Hawk procurement was more than 50% of the

Army's rotary wing aircraft procurement.

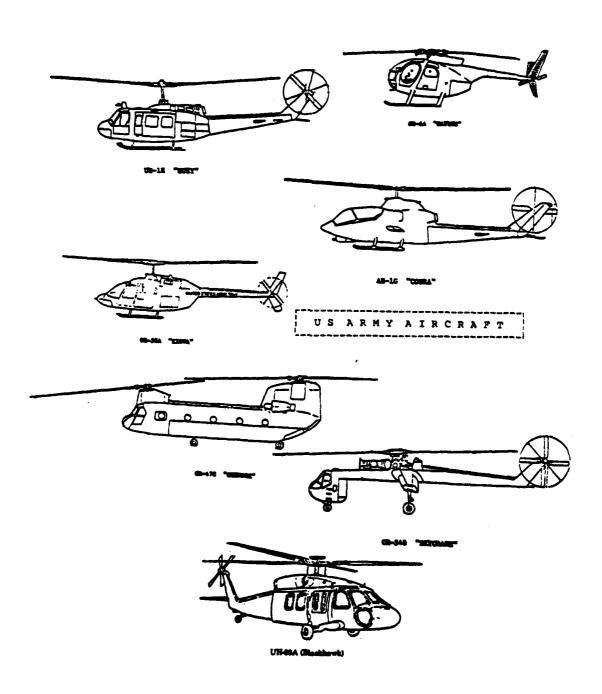
I. Additional Publications Relating to this Report

The Office of the Comptroller, Cost Analysis Division, can supply the following publications which may be of assistance in using and interpreting these inflation indices:

- CM 82-2 Inflation Indices, An Introduction to Basic Theory
 and Their Application with sample problems. Nov 1981
- CM 83-8 The Historical Inflation Program, for Army Aircraft
 Abbrev Ed., (Expected April 1983).
- CM 83-2 The Troop Support Inflation Program Jan 1983.

US ARMY HELICOPTER MATERIAL DATA

UNITED STATES ARMY AVIATION



Air Order of Battle

United States Army - Quantities and Types of Fielded Aircraft

ROTARY WING AIRCRAFT

As of 31 December 1982

System <pre>Designation</pre>	Popular Name	Approx Empty Wt.	No. of Aircraft	Percent of Fleet
AH-1	"COBRA"	5,800 lbs.	1,028	13.1%
UH-1	"HUEY"	5,100 lbs.	3,726	47.2%
OH-6	"CAYUSE"	1,200 lbs.	373	4.7%
OH-58	"KIOWA"	1,750 lbs.	1,971	25.0%
CH-47	"CHINOOK"	19,500 lbs.	404	5.1%
CH-54	"SKYCRANE"	19,800 lbs.	72	.9%
UH-60A	"BLACK HAWK"	10,500 lbs.	315	4.0%
AH-64A*	"ADV. ATTACK"	10,400 lbs.	0	<u> </u>
			7,889	100.0%

Sources:

Field Manual 101-20, HQ Dept of the Army, January 1979.
 World Combat Aircraft Directory, Doubleday & Company, 1976.

Army Aircraft Inventory Status and Flying Time, HQ, USA-TSARCOM, 31 Dec 82, p. 15 (Unclassified)

^{*}Six aircraft in inventory as prototypes. Fielding of Aircraft to begin in February 1984.

MESAV-CCE

31 July 1973

MENDRANDOM INDU: Mr. Gerald Dockins, Acting Chief, Estimates and Studies Branch

POR: Mr. Edward P. Laughlin, Chief, Cost Analysis Division C

SUBJECT: Material Composition Analysis of U.S. Army Belicopters, July 1973

1. On 6 Jume 1973, this office received a request from Mr. W.J. Tropf, AMC Comptroller Office, Cost Amalysis Division, for the material composition of a UN-1H helicopter. On 18 Jume 1973, Chief, AVSCOM Comptroller Office, Cost Amalysis Division requested a similar analysis be performed on the following Army belicopters:

9-17.

Ø₽-64.

OH-58A.

AH-16.

CH-54B.

2. A search of the technical data files and aircraft drawings failed to produce the desired date. The analysis was completed with the assistance of AVSCON Systems Engineering Division, Directorate of Rolfs and pertinent U.S. Army Plant Activities. Contractors were also contacted during the data search, and others. The data obtained are a combination of expert opinion, engineering estimates and contractor data obtained under previous contracts.

The following Cost Analysis personnel were assigned to this project:

Assigned To Aircraft System Gerald Dockins Sames Cadell John Thilmany

Gerald Dockins/James Cadell Gerald Dockins/James Cadell James Cadell

CH-13 CH-57 CH-57 CH-57 CH-58 CH-58

31 July 1973 SURJECT: Material Composition Analysis of U.S. Army Melicopters, July 1973

4. Copies of the Material Composition Analysis have been placed in the fellowing files:

a. A new file folder titled "Material Composition Analysis".

b. A complete copy of the findings placed in the file folder titled "Inflatica".

c. A separate file of the findings relating to turbine engines has been created.

5. Summary Tables and Material Composition Analyses are inclosed.

Lune M. Cally

JAMES N. CADELL Math-Stat

13

MATERIAL COMPOSITION OF US ARMY HELICOPTERS

Material Composition Analysis for U.S. Army Turbine Engines Material (Pounds)

Ungine Model	Dry Weight	Alupinus	Steel	Hagnesium	Titanium	Copper	Nickel Alloy	Hommetale	Steiniese Steel	Stee! Alloy
153-L-13	527	79	316	60	26	,	0	23	•	0
163-A-5A	130		100	26				,	•	0
T63-A-700	130		100	26			٥	,	0	•
795-L-70	590		510	50	20	10	0	0	•	•
T73-P-700	981	1	0	0		0	290		596	94
7700-GB-700	423	124	83	•	16	1	183	,		,

Material Composition Analysis for U.S. Army Helicopter Airframes Material (Pounda)

Aircraft Model	Airfreme Weight	Aluminum	Steel	Hegnes i um	Titanium	Copper	Brass	Bronse	Lond	Tungeton	Hickel Alloy	Remotal to
AR-1G	4,867	1,009	1,464	136	82	590	0	0	216	0	•	570
un-1# }	4,446	1,500	1,402	200	44	400	100	0	100	•		700
UM-60A	6,841	3,040	3,035	352	901	112	2	z	28	•	10	1,363
OW-6A	1,025	466	109	20	ı	30	23	,	0	1	25	147
OH-56A	1,448	536	434	29	15	101	0	0	43	•		290
CR-47C	9,651	4,156	3,484	602	11	328	2		0	23		1.037
CR-548	17,003	8,928	2.480	77	970	516	20	23	1		209	4,384

I: included in figures for copper.

Material Composition Analysis of Army Helicopters Material (Pounds)

Aircraft Hodel	Empty Weight	Aluntaun	Steel	Magnes Lum	Titenim	Copper	Brass	Bronse	Lead	Tungston	Hickel Alley	Permeta) (c
AR-IG	5,394	1,888	1,780	216	108	593	0	0	216	0	۰	593
UM-111	4,973	1,579	1,718	200	70	480	100		100	•		726
W-60A	10.679	3,647	3,404	406	1.057	130	2	2	32	0	223	1,500
OR-6A	1,163	444	216	46		30	23	,		1	25	150
OR-58A	1,586	536	343	55	15	101			43	•		293
OR-47C	20,483	8,312	7,989	1,304	63	676	4	16		45	•	2,074
CR-548	19,765	8,931	3,860	72	970	516	20	23			796	4,504

I: included in figures for copper.

AIRCRAFT LABOR AND MATERIAL BREAKDOWN

SUMMARY OF AIRFRAME AND ENGINE CIR DATA¹

	Airframe	Engine
Labor	62.08%	40.85%
Material	37.92%	59.15%
Total Cost	100.00%	100.00%
Raw Material	41.88%	70.58%
Purchased Equipment	58.12%	29.42%
	100.00%	100.00%

NOTES:

- (1) Airframe factors were obtained from a sample of 15 CIR reports and other documents representing the AH-1, CH-47, CH-54, OH-6, OH-58, and UH60A aircraft systems.
- (2) Engine factors were obtained from a sample of 14 CIR reports and other documents representing 12 different turbine engine configurations procured from Lycoming, Allison, General Electric, and Pratt & Whitney.

1. From <u>HISTORICAL INFLATION INDICES FOR ARMY AIRCRAFT</u>
US Army Aviation Systems Command, St. Louis, 1974, p. 11.

TECHNICAL SECTION

- IV. ANALYSIS: (TECHNICAL SECTION).
- A. <u>Chronology</u>. Previous efforts related to the development of inflation indices include <u>Aerospace Price Indexes</u> by H.G. Campbell, RAND Corporation, December 1970 (Reference 1) and two cost research reports: <u>Historical Inflation Indices for Army Aircraft</u>, Cost Analysis Division, Office of the Comptroller, U.S. Army Aviation Systems Command, September 1973 (Reference 4), and <u>Historical Inflation Indices for Army Aircraft</u>, Cost Analysis Division, Office of the Comptroller, U.S. Army Aviation Systems Command, August 1974 (Reference 5).
 - 1. Characteristics of the RAND Report.
- a. Specific Producer Prices and Price Indexes (Reference 8) and Employment and Earnings (Reference 2) data have been selected as proxy series for similar commodity and labor categories experienced in the procurement of Army aircraft. Aircraft inflation indices are constructed from a weighted average of these proxy series. The weighting factors for this average are derived from estimates of the relative contribution to the total aircraft cost made by each component (commodity or industry labor group) comprising the index. The index is thus a "cost-weighted" series.
- b. A 25 percent compounded annual rate for growth of overhead ratios is assumed.
 - c. No adjustment is made for productivity increases.
 - d. Indices are developed on a calendar year basis.
 - 2. Characteristics of the September 1973 Cost Research Report.

- a. As with the RAND report, aircraft inflation indices have been constructed from a weighted average of <u>Producer Prices</u> and <u>Price Indexes</u> and <u>Employment and Earnings</u> data selected as proxy series for their similarity to those commodities and labor categories experienced in the procurement of Army aircraft. Weighting factors are proportional to the relative physical weights or masses, rather than to the relative costs of commodities comprising the "composite material" portion of the index as in the RAND report. Thus, the "composite material" portion of the index represents a "weight-weighted" series.
- b. Like the RAND report, a 2½ percent annual growth in the overhead ratio is assumed.
 - c. No adjustment is made for productivity increases.
 - d. Indices are developed on a calendar year basis.
- e. For years for which certain specified Producer Price Indexes were unavailable, data has been projected from adjacent years.
 - 3. Characteristics of the August 1974 Research Report.
- Employment and Earnings data have been selected as proxy series most similar to those commodities and labor categories experienced in the procurement of Army aircraft. The indices have been constructed from a weighted average of these proxy series utilizing the weighting factors used in the September 1973 Cost Research Report. The "composite material" portion of the index represents a "weight-weighted" series.

- b. Unlike RAND and the September 1973 Cost Research Report, no adjustment for overhead growth is assumed.
 - c. No adjustment for productivity increases is assumed.
- d. Indices have been extended to FY 1974 by assuming that data for the September 1973 Cost Research Report represented December and hence the fiscal year midpoint, rather than the annual average, of each calendar year.
- e. For years for which certain specified Producer Price Indexes were unavailable, data has been projected from adjacent years.
- B. <u>Data Sources</u>. Data sources for this report are <u>Producer Prices</u> and <u>Price Indexes</u> (reference 8) and <u>Employment and Earnings</u> (reference 2). To insure that the latest revisions were incorporated into the data base, data was obtained from the Kansas City Regional Office, Bureau of Labor Statistics, and annual supplements to <u>Producer Prices and Price Indexes</u>. For <u>Employment and Earnings</u>, data for any given month was obtained from the latest available source. Data used in this report are displayed in Appendices D, E, G, and H.

C. Methodology.

1. Overhead and Productivity Adjustments. On the basis of data covering a ten year period, the RAND report concluded that there exists a secular growth trend of 2½ percent per year in the production overhead rate. The report also concluded that there has been little, if any, improvement in productivity to counteract the observed trend in overhead growth. This conclusion appears to

be unwarranted, particularly in light of productivity gains recorded (as measured by Industrial Production Indices) for similar sectors of industry. Thus, in order not to unduly bias the results of the analysis, this report makes no adjustment for either overhead growth or improvements in productivity.

2. <u>Calculation of Weighting Factors</u>. From a number of Cost Information Reports, the following weighting factors were developed and reported in the September 1973 Cost Research Report.

For the Airframe:

Purchased Equipment = (.378) Raw Material + (.622) Labor 3728

Total Material = (.582) Purchased Equipment + (.418) Raw Material

Total Airframe = (.378) Total Material + (.622) Labor 3721

For the Engine:

Purchased Equipment = (.599) Raw Material + (.401) Labor 3728

Total Material = (.295) Purchased Equipment + (.705) Raw

Material

Total Engines = (.599) Total Material + (.401) Labor 3724

And for Avionics:

Total Avionics = (.315) Material + (.685) Labor 367X

In the previously published indices, the weighting factors used to develop the material portion of the indices were made proportional to the relative physical weights of the various commodities used in the construction of the aircraft. The material portion of these indices thus represent a "weight-weighted" series. In order to be consistent with the intended

purposes of an inflation index, the methodology in this program uses index weighting factors proportional to the numerical products obtained from multiplying the relative physical commodity weights by the appropriate base year cost per pound. This yields a "cost-weighted" index giving more weight to such expensive commodities as titanium. Unfortunately, however, price per pound data are not published in Producer Prices and Price Indexes for each of the commodities used in constructing the indices. To overcome this difficulty, the per pound price was estimated from the available data of the most closely related commodities. To minimize the effect from related commodities which have relatively little economic impact, each price per pound estimate was developed from a weighted average of available data utilizing the Bureau of Labor Statistics 1975 revised relative weights published in the 1975 Annual Supplement to Producer Prices and Price Indexes. available data then constitutes a weighted sample from which a surrogate price per pound is computed for the Producer Price series in question. See Appendix A for the computations for the derivation of these revised weighting factors, along with their associated cost contribution per pound.

3. Construction of Indices.

a. Calendar Year 1967 was taken as the base for these indices because this year represents the approximate midpoint of the period for which the data supports the development of each of the indices, including those which account for avionics.

Furthermore, 1967 conforms to the base used by the Bureau of Labor Statistics for Producer Price Indexes.

- b. Appendix B contains the current Producer Price Index series, Employment and Earnings series, and the associated weighting factors used in the construction of the indices published in this report. Since some of these series have been in existence for only a limited time, other closely related series have been substituted with appropriate mathematical adjustments to insure continuity of the indices. This technique is considered perferable to the synthesis of data by projection from adjacent years. Appendix C depicts the historical flow and identifies the effective dates of series conversions, for the Producer Price Index and the Employment and Earnings data used in the development of the indices published in this report.
- c. The term "aggregate" has been selected to indicate inflation indices applicable to the combined Airframe and Engine (aggregate Air Vehicle Excluding Avionics) and to the combined Airframe, Engine, and Avionics (Aggregate Air Vehicle Including Avionics) to avoid confusion with the term "composite" as in "composite escalation indices". Aggregate indices are based upon a standard 70-20-10 weighting (see Reference 6) of the Airframe, Engine and Avionics indices respectively. Aggregate indices are intended for the adjustment of historical cost data for which the distribution of costs for the Airframe, Engine, and Avionics components is unavailable.
 - d. A section depicting the raw material portion of

the inflation indices is published as Appendix I. It is intended for applications requiring greater accuracy in labor cost escalation. Appropriate labor indices can be obtained from the Bureau of Labor Statistics Employment and Earnings series (Reference 2) as follows:

Labor Category	1967 SIC Code	1972 SIC Code	Industry
Airframe Contractor	3721	3721	Aircraft
Airframe Subcontractor	3723,9	3728	Other aircraft part & equipment
Engine Contractor	3722	3724	Aircraft engines & engine parts
Engine Subcontractor	3723,9	3728	Other aircraft parts & equipment
Avionics	3674,9	367X	Other electronic components
Aggregate Air Vehicle Excluding Avionics	372	372	Aircraft and parts

With appropriate adjustments, labor cost data from specific geographic areas, manufacturers, or plants can be used. The computational formulas for labor cost indexes are given on page B-5 in appendix B.

- e. The Basic Computational Methodology is as follows:
- (1) For Components: Airframe, Engine, and Avionics.
- (a) Calendar year indices are computed using sum of weighted calendar year labor and material indices.
- (b) Fiscal year indices are computed in a manner similar to calendar year, but the yearly fiscal averages are generated from the monthly data.
 - (c) Quarterly indices are computed by averaging three

months data from the monthly data set.

(d) Monthly indices are computed by direct calculation using monthly data. It is a weighted average of monthly figures computed using the same methodology as in computing the calendar year indices.

For additional information, see Appendix B.

(2) Aircraft System Cost

The inflation indices for "Aggregate Vehicle" and Aggregate Vehicle without Avionics" are produced by combining the three separate indices:

Component	Relative Weight
Airframe Index	70%
Engine Index	20%
Avionics Index	10%
	- The state of the
Aggregate Vehicle	100%
Component	Relative Weight w/o Avionics
Component Airframe Index	
	w/o Avionics
Airframe Index	w/o Avionics 78%

b. Reduced form equations are displayed in Appendix B, page B-6.

V. DESCRIPTION OF COMPUTER PROGRAM AND ASSOCIATED APPENDICES.

The Historical Inflation Program is a computer program used to generate historical inflation indices for Army aircraft and their major subsystems. Appendices D and G contain the annual data used by the program, while the monthly data, commencing July 1967, are in Appendices E and H. Producer Price Index and Earnings data in these Appendices have been arrayed into columns with the same numerical code sequence used in Appendix B. Historical inflation indices and factors are published in Appendix F. Fiscal Year, quarterly, and monthly indices have been developed from the appropriate monthly data. A section containing the raw material portion only of these indices is published as Appendix I. The labor portion of these indices may be obtained by applying the methodology described on pages B-2 through B-5 to the data contained in appendices D and E.

VI. SENSITIVITY ANALYSIS

Many considerations are important when constructing Historical Indices for tracking purposes. These certainly include the following:

- a. The nature of the items chosen to comprise the index.
- (1) How typical or representative the items are.
- (2) How closely the proxy items approximate the actual items, if indices for the actual items are not obtainable.
- (3) The number of items used, and the detail in the analysis which produced the indices.
- b. The determination of the percent contribution to cost "Cost Drivers".
 - c. The weighting factors employed in the overall analysis.

A difficult problem confronting cost analysts, who must determine the validity of an historical index for tracking purposes, relates to aggregate labor/material weighting factors. In tracking major weapons systems, the ratio is often stated as say 40/60 - that is 40 percent material and 60 percent labor - as percent contributions to cost. Because it is difficult for analysts to determine the "correct" aggregate mix of labor and material, being external to the project, the aggregate split is certainly of interest.

The value for any index depends on three factors:

- 1. The number of factors employed, and the quality and depth of the analysis.
- 2. The values for each component of cost used in the construction of the index.
- 3. The weights, or levels of importance, given to the factors, individually and collectively.

The objective of this sensitivity analysis is to shed some light on the way in which the aggregate labor/material split affects the index, which has been a controversial issue for some time. Using a set of recursive linear equations, the effect on the historical inflation index, for airframe, resulting from varying the aggregate weighting scheme was calculated, in both raw and percentage terms. The calculations were made using a Wang system 2200 minicomputer, and a sample printout follows. The results provide evidence that the key to a successful index resides in item a. (3) the number of items used, and the quality and detail in the analysis used in preparing the index. Because wages are often tied to the Producer Price Index, or other price indices, in labor agreements, it is not surprising that aggregate weighting percentages for labor and material might not be an extremely sensitive issue. However, the calculations provide strong support

for the position that the identification of cost components and the depth and quality of detail in an analysis are of paramount importance, when developing an index to be used in controlling the cost of a major weapon system.

CHANGET TO THE STATE OF ALTERNATION OF ALTERNATION

GROSS MATL	GROSS LABOR	PURE MATL	PURE LABOR	NEM INDX	CURR INDX	PERCENT CHANGE
37%	. 6220	2411	7588	2. 1471	2. 1470	Ø. 99
200	. 8666	. 1068	. 8931	2. 1659	2. 1470	ø. 88
256	. 7500	. 1408	. 8591	2. 1611	2. 1470	මි. ප්සි
ି ଅଧିକ	. 7000	. 1777	. 8222	2. 1559	2. 1470	Ø. 41
256	. 6500	2175	. 7824	2. 150 4	2. 1470	ø. 15
400	. 6000	. 2603	. 7396	2. 1444	2. 1470	- 0.12
450	5500	. 3059	. 6940	2. 1380	2. 1470	- Ø. 41
500	. 5000	. 3545	. 6455	2. 1312	2. 1470	- Ø. 73
. 556	4500	. 4059	. 5940	2. 1239	2. 1470	- 1.07
සිමිම	. 4000	4603	. 5 396	2. 116 3	2. 1470	- 1.42
<i>6</i> 59	3500	. 5175	. 4824	2. 16 83	2. 1470	- 1.80
?මග	. 3000	5777	4222	2. 0998	2. 1470	- 2.19
75 6	. 2599	. 6408	. 3591	2. 0910	2. 1470	- 2, 60
. පමම	. 2000	. 7063	. 2931	2. 0817	2. 1470	- 3, 03

510 2721 - 7,700 SIC 3723.9 - 6,920 NEW MAT IND = .4920

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- 2. Employment and Earnings. Washington, DC: US Department of Labor, Bureau of Labor Statistics
- Field Manual 101-20, <u>Army Aviation Planning Manual</u>, Washington D.C.: Headquarters, Dept of the Army, January 1979.
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 St. Louis, MO: US Army Aviation Systems Command, Office of the Comptroller, Cost Analysis Division, September 1973.
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 St. Louis, MO: US Army Aviation Systems Command, Office of the Comptroller, Cost Analysis Division, August 1974.
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- 3. <u>International Financial Statistics</u>. Washington, DC: <u>International Monetary Fund</u>, <u>Monthly</u>.
- 4. Letter, subject: <u>Inflation Guidance</u>. Alexandria, VA: US Army Materiel Development & Readiness Command, Office of the Comptroller, Cost Analysis Division, 18 January 1983.
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 Estimates. Washington, D.C.: Headquarters Department
 of the Army, Office of the Comptroller of the Army,
 Cost Analysis Division, 9 September 1982.
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APPENDIX A

Computations For The Derivation

Of Revised Weighting Factors

For The Historical Inflation Program

COMPUTATIONS FOR THE DERIVATION OF REVISED WEIGHTING FACTORS FOR THE HISTORICAL INFLATION PROGRAM

1967 Price Per Pound	.6216	1.3752	5.2926
Product 3	. 073 . 03774 . 03764 . 07478		
Weight ²	. 121 . 082 . 048 . 108		
1967 Price Per Pound	.6033 .4602 .7841 .6924	1.3752	5.2926
Commodity	COPPER AND BRASS MILL SHAPES Cartridge Brass Strip, 70-30 Alloy Yellow Brass Rod(62-35-3 Alloy) Yellow Brass Tube(70-30 Alloy) Copper Sheet or Strip	MONEL SHEET, CR 400 ALLOY	TITANIUM MILL SHAPES ⁵ Titanium Bar, Ground, 6AL-AV
PPI CODE	10 25 02 31 32 33 55	10 25 04 63	10 25 05 25

Weighted4

Capitalized and Underlined Commodity Titles indicate PPI Series actually used in the Historical Inflation Program. NOTES:

Weight is Bureau of Labor Statistics revised relative Weight for the Producer Price Index. Source: 1975 Annual Supplement to Producer Prices and Price Indexes.

Product = $(1967 \text{ Price Per Pound}) \times (Weight)$.

. Weighted 1967 Price Per Pound = Product Weight

1967 Titanium Bar price per pound computed by utilizing Titanium Sponge index as surrogate for 1967 - Dec 1970. Titanium Mill Shapes index established December 1970. Titanium Sponge index for December 1970 is 95.5. ۍ.

Tracked using proxy PPI Code 10250153 beginning in Jan 1982. •

COMPUTATIONS FOR THE DERIVATION OF REVISED WEIGHTING FACTORS FOR THE HISTORICAL INFLATION PROGRAM

PP1 Code	СОМНОВІТУ	Contrib. to Weight	Contrib. to Weight Engine	1967 Cost Per Pound	(DOLS) Contr. to cost per lb Airframe	(bols) Contr. to cost per lb Engine	Percent Contrib. to cost	Percent Contrib. to cost Engine
07	Rubber and Plastic Products	.17	.012	.2376	.04039	.00285	.0211	.0023
10 17 07 11	Sheets, Carbon Steel	.055		.0737	.00405		.0021	
10 13 02 64	Sheets, C.R., Stainless		.584	.5531		.32301		.2625
10 15 01 41	Steel Castings	.22		.0497	.01093		.0057	
10 15 13 51	Closed Die Forgings		.146	.0497		.00725		6500.
10 22 01 27	Lead, Pig, Common	.01		.14	.0014		.0007	
10 22 01 51	Magnesium, Pig Ingot	.033	.077	3595.	.01186	.02768	.0062	.0225
10 25 01 01	Aluminum Sheet	.256	.021	.4185	.10715	.00879	.0560	1,000.
10 25 01 41	Rod, Screw, Machine Stock	.043	.004	.6315	.02715	.00253	.0142	.0021
10 25 01 17	Extrusion, Solid Circle Size 4 to 5	.128	.01	.6315	.08083	.06632	.0422	.0051
10 25 02	Coprer and Brass Mill Shapes	. 049	.005	.6216	.03046	.00311	.0159	.0025
10 25 04 63	Monel Sheet, CR 400 Alloy	.011	.122	1.3752	.01513	77791.	6200.	.1364
10 25 05	Titanium Mill Shapes	.025	610.	5.2926	.13231	10056	.0691	. 0817
		1.000	1.000		\$.46167	\$.64986	.2411	.5281

(52.811)

(24.114)

EXPLANATORY NOTES FOR REVISED WEIGHTING FACTORS

HISTORICAL INFLATION PROGRAM

NORMALIZATION FACTOE
×
1967 COST PER POUND
×
CONTRIBUTION TO WEIGHT
ij
CONTRIBUTION TO COST

Contributions to cost and weight are percentages in decimal form. NOTES:

Percent Contribution to Cost	Material Cost Per Pound
Normalization Factor =	
5.	

a. Engine Normalization Factor =
$$\frac{.5281}{.64986}$$
 = .813
b. Airframe Normalization Factor = $\frac{.2411}{.46167}$ = .522

Coefficient for Titanium reduced by a factor of .955 in December 1970. Titanium Sponge Index replaced by Titanium Mill Shape Index. . .

COMPUTATIONS FOR THE DERIVATION OF REVISED WEIGHTING FACTORS FOR THE HISTORICAL INFLATION PROGRAM

PP1 Code	COMMODITY	Percent Contrib to Cost Airframe	Percent Contrib to Cost Engine	High Tech Adj. Factor Airframe	High Tech Adj. Factor Engine	High Tech Percent Contrib to Cost	High Tech Percent Contrib to Cost Engine
07	Rubber and Plastic Products	.0211	.0023	1.004	.964	.0181	.0014
10 17 07 11	Sheets, Carbon Steel	.0021	,	1.010	ı	.0019	ı
10 13 02 64	Sheets, C.R., Stainless	ı	.2625	1	.967	•	.1631
10 15 01 41	Steel Castings	.0057	ı	1.010	ſ	.0050	i
10 15 13 51	Closed Die Forgings	ı	.0059	ſ	716.	i	.0038
10 22 01 27	Lead, Pig, Common	.0007	ŧ	.921	ı	9000.	1
10 22 01 51	Magnesium, Pig Inyot	7900.	.0225	1.000	.922	.0053	.0134
10 25 01 01	Aluminum Sheet	.0560	.0071	.992	1.118	.0474	.0051
10 25 01 41	Rod, Screw, Machine Stock	.0142	.6021	.992	1.118	.0120	.0016
10 25 01 17	Extrusion, Solid Circle Size 4 to 5	.0422	.0051	1.010	1.118	.0364	.0037
10 25 02	Copper and Brass Mill Shapes	.0159	. 0025	.927	.970	.0126	.0016
10 25 04 63	Monel Sheet, CR 400 Alloy	6200.	.1364	1.050	3.220	.0071	.2822
10 25 05	Titanium Mill Shapes	0990.	.0817	1.640	1.000	.0922	.0525
			:			1	:

(23.80%) (52.81%)

.5281

.2380

.5281

.2380

EXPLANATORY NOTES FOR REVISED WEIGHTING FACTORS

HI-TECH COMPUTATIONS

NORMALIZATION FACTOR
×
HI-TECH ADJUSTMENT FACTOR
×
PERCENT CONTRIBUTION TO COST
u
HI~TECH CONTRIBUTION TO COST

Old Material Percent by Weight Hi-Tech Adjustment Factor = New Material Percent by Weight NOTES:

i.e. engine monel sheet is 4.25% by weight under the new bill of materials and 1.32% under the ole, so the Adjustment Factor = $\frac{4.25\%}{4.25\%}$ = 3.22

Normalization Factor = Sum of Old Contributions to Cost Sum of New Contributions to Cost 2.

Engine Normalization Factor = $\frac{.5281}{.8219}$ = .6425

b. Airframe Normalization Factor = .2380 = .8520

Normalization Factor reduces total material percentages to .2380 (Airframe) and .5281 (Engine) so that when combined with labor percentages of .7620 (Airframe) and .4719 (Engine) cost contributions sum to unity. <u>ب</u>

i.e. .2380 + .7620 = 1.000 and .5281 + .4719 = 1.000

APPENDIX B PRODUCER PRICE INDEXES AND EARNINGS SERIES USED IN HISTORICAL INFLATION PROGRAM WITH REVISED WEIGHTING FACTORS

PRODUCER PRICE INDEXES AND EARNINGS SERIES USED IN HISTORICAL INFLATION PROGRAM AND REVISED WEIGHTING FACTORS

Var	PPI Code	Commodity	Airframe	*HI-TECH Airframe
(1)	07	Rubber and Plastic Products	.0211	.0181
(2)	10 17 07 11	Sheets, Carbon Steel	.0021	. 0019
(3)	10 13 02 64	Sheets, C.R., Stainless		
(4)	10 15 01 41	Steel Castings	.0057	.0050
(5)	10 15 13 51	Closed Die Forgings		
(9)	10 22 01 27	Lead, Pig, Common	.0007	9000.
(7)	10 22 01 51	Magnesium, Pig Ingot	.0062	.0053
(8)	10 25 01 01	Aluminum Sheet	.0560	.0474
(6)	10 25 01 41	Rod, Screw, Machine Stock	.0142	.0120
(10)	10 25 01 17	Extrusion, Solid Circle Size 4 to 5	.0422	.0364
(11)	10 25 02	Copper and Brass Mill Shapes	.0159	.0126
(12)	10 25 04 63	Monel Sheet, CR 400 Alloy	6200.	.0071
(13)	10 25 05	Titanium Mill Shapes	0990.	. 0922
(14)	11 78	Electronic Components		
	SIC Code	Industry		
(15)	367X	Other Electronic Components		
(16)	3721	Aircraft	.6220	.6220
(11)	3724	Aircraft Engines and Engine Parts		
(18)	3728	Other Aircraft Parts and Equipment	.1369	.1369

1.0000

1.0000

* Includes UH-60A BLACK HAWK Aircraft.

PRODUCER PRICE LIDEAL AND ENTRY OF SHOUSED USED IN HISTORICAL INFLATION PROGRAM AND REVISED WEIGHTING PACTORS

Var	PPI Code	Commodity	Engine	*HI-TECH Engine
(1)	0.0	Rubber and Plastic Products	.0023	.0014
(2)	10 17 07 11	Sheets, Carbon Steel		
(3)	10 13 02 64	Sheets, C.R., Stainless	.2625	.1631
(4)	10 15 01 41	Steel Castings		
(5)	10 15 13 51	Closed Die Forgings	.0059	.0038
(9)	10 22 01 27	Lead, Pig, Common		
(7)	10 22 01 51	Magnesium, Pig Ingot	.0225	.0134
(8)	10 25 01 01	Aluminum Sheet	1,0071	.0051
(6)	10 25 01 41	Rod, Screw, Machine Stock	.0021	.0016
(10)	10 25 01 17	Extrusion, Solid Circle Size 4 to 5	.0051	.0037
(11)	10 25 02	Copper and Brass Mill Shapes	.0025	.0016
(12)	10 25 04 63	Monel Sheet, CR 400 Alloy	.1364	.2822
(13)	10 25 05	Titanium Mill Shapes	.0817	.0525
(14)	11 78	Electronic Components		
	SIC Code	Industry		
(15)	367x	Other Electronic Components		
(16)	3721	Aircraft		
(17)	3724	Aircraft Engines and Engine Forts	.4010	.4010
(18)	3728	Other Aircraft Parts and Equipment	.0709	6970.
)u] *	Includes UH-69A/F70v Eagine	gine	1.0000	1.0000

PRODUCER PRICE INDEXES AND BARNINGS SERIES USED IN HISTORICAL INFLATION PROGRAM AND REVISED WEIGHTING FACTORS

COMPUTATIONAL FORMULAS FOR LABOR COST INDEXES

expressed in dollars per hour, labor costs over time must be converted to indices before calculations can be made. The dollar per hour to index conversions for the labor categories are done wage rates by Standard Industry (SIC) Codes, and are reported on a regular basis in Employment The data for cost of labor services is supplied by the Bureau of Labor Statistics, as hourly and Earnings. Because material indices are expressed as indexes, base 100, and wages are as follows:

U C	= 367X Index	= 3721 Index	= 3724 Index	= 3728 Index
		100%		100%
4 5.1	~	×	×	
CY 1967 Hr. Wage	\$ 2.34 X 100%	\$ 3.49	÷ \$ 3.42 X 100%	÷ \$ 3.35 X
	•) •	.).	.1.	.1.
	Current Hr. Wage	Current ÷ \$ 3.49 X	Current Hr. Waqe	Current Hr. Wage
				_
Industry	Electronic Components	Aircraft Production	Aircraft Engines & Engine Parts	Aircraft Equipment
SIC	367X	3721	3724	3728
Var	(15)	(16)	(17)	(18)

REDUCED FORM EQUATIONS

Airframe =
$$.0211(V-1) + .0021(V-2) + .0057(V-4) + .0007(V-6) + .0062(V-7)$$

+.056(V-8) + .0142(V-9) + .0422(V-10) + .0159(V-11) + .0079(V-12)

$$+.0660(V-13) + .622(V-16)(100/3.49) + .1369(V-18)(100/3.35)$$

.3150(V-14) + .6850(V-15)(100/2.34) ij Avionics

+.401 (V-17) (100/3.42) + .0709 (V-18) (100/3.35)

HI-TECH REDUCED FORM FQUATIONS

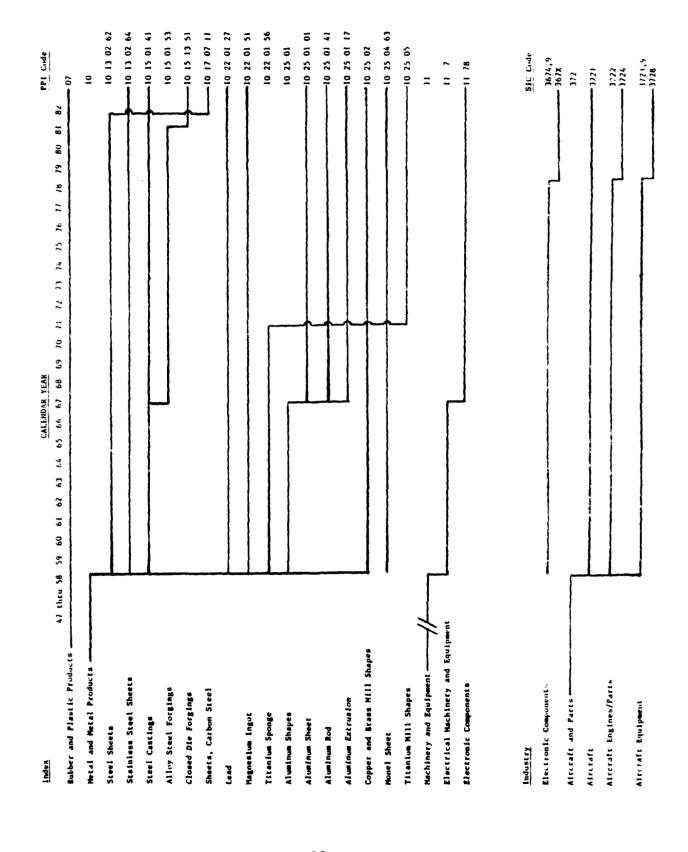
.3150(V-14) + .6850(100/2.34) U HI-TECH Avionics

Variables (V-1) thru (V-18) are defined on page B-2

APPENDIX C

HISTORICAL FLOW OF PRODUCER PRICE INDEXES AND
EARNINGS SERIES USED IN HISTORICAL INFLATION
PROGRAM WITH REVISED WEIGHTING FACTORS

Mistorical Flow of Producer F., . . undexessand Earnings Series Used in Historical Inflation Program



APPENDIX D Annual Data for The Historical Inflation Program for U. S. Army Rotary Wing Aircraft

CALEGOAR YEAR JATA

510312	1.374	1.467	1.56.1	1.037	1.760	1.896	1.996	2.07"	2.166	2.273	2.350
	24.96	62.54	(3.6n	10£ • 3.1	13.81	15.90	76.36	16.91	82.10	19.20	91.66
10-144	70.50	72.30	71.56	55.90	105.40	45.5A	69.10	50.40	162.40	173.60	143.40
Č	1347	1998	1349	1356	1951	1952	1953	1954	5961	1936	1961

5	0.37x 9.09.LER	, ,	130ce2 136204 CP SIL SIRLS	11.2.4 CASH	5 16:151 FOR 3E	22.4111 LE 50	114 TEH 220151 946NES	1415	9 25, 113	14 254117 FXTRU	785760 785760	12 25.1463 43.161	15 2005 XX 11-91L	14 11 75 X X	15 15 61.6.01 55.7x	16 ACF 1 E	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	13 01853 372
1358	105.39		93.10 125.70	93.24	15 S S S S S S S S S S S S S S S S S S S	de. lu	1 de a u s	137.00	117.64	117.ca 137.cb	7.1.1	74.53	144.33	94.90	1.7.1	6.51	2.31	
1 355	102.94		54.70 121.53	14.36	9£.44B	67.24	1 11 0 0 11	1,60.01	136.60	1 ° 6 • if	3 6 F	10.51	122.40	99.50	11.11	2.64	3.64	2065
1 360	113.13		94.70 120.20) t. • bil	96.40	85.20	190.061	110.66	114.80	116.60	81.70	02.10	117.90	98.20	1.46	2.71	2.73	5.54
1961	94.26		94.74 118.60	97.08	30.7e	17.64	100.3	111.50	1111.30	1111.50	75.16	89.44	108.1.	98.20	1.93	2.78	2.61	2.70
1362	80.33		94.73 115.40	91.43	97.60	04.7L	100.03	1.18.7.	196.70	108.70	13.94	91.6.l	101.44	96.70	1.97	2.07	2.91	2 • b C
1965	96.40		96.34 147.18	97.8"	97.03	79.60	100.03	102.90	102.50	102.90	73.40	91.60	97.50	95.70	2.01	2.95	2.99	2.05
1564	95.50	96.00	94.40	97.19	97.10	97.00	106.001	101.40	171.40	101.40	78.50	40.64	97.30	92.10	2.05	3.00	3.03	2.96
1565	95.9u	98.f.3	91.43	98.13	90.16	114.30	1.30.00	04.66	09.40	99.40	66.10	90.00	98.80	95.10	2.14	3.15	3.17	3.08
1966	67.80	98.74	91.64	19.64	97.40	107.20	100.001	38.5A	98.50	98.50	99.30	54.29	100.00	97.10	2.21	3.54	3.32	3.21
1367		66.60 106.10 103.501	16.1.33	139.69	10.0.01	130.00	190.00	139.00	103.00	100.10	101.00	131.00	100.00	140.00	2.34	3.49	5.42	3.35
1368		103.40 104.70 103.10 105.70 102	103.10	105.70	102.00	94.60	100.00	142.40	95.80	102.40	107.30	105.20	94.50	99.20	5.49	3.64	3.05	3.53
Ä 1569		105.30 109.c0 112.5u	112.5u	115.40	108.10	10c.50	100.00	109.70	51.06	112.10	119.26	112.20	98.00	100.70	2.61	3.50	3.87	3.16
1574		13r - 30 116 - 40 130 - 9.	130.9.	117.50	117.10	112.10	1 30.06	110.60	93.40	120.001	136.00	132.10	95.50	101.00	2.18	4.17	4.10	3.59
11311		169-18 125-43 135-84 125-36 122-9	135.09	125.30	122.93	บา • 66	102.70	1:16.70	93.40	121.40	118.69	139.70	1:12.90	04.501	2.91	4.36	4.36	4.15
1972		189.38 135.58 125.40 129.88	125.40	123.00	130.50	109.00	103.60	134.40	93.50	123.20	124.50	14.1.40	107.00	105.40	3.02	4.74	4.14	4.37
1213		112.40 135.34 122.19	122.19	156.20 135.9	135.90	117.66	1.70.44	r5.23	93.40	125.10	141.70	144.21	109.20	104.40	5.16	5.13	50°5	4.60
181	13c.20	13c.20 167.cf 157.lu 165.9u 161.8	157.14	163.94	161.86	159.10	173.20	130.40	120.60	150.90	102,70	175.00	132.50	1111.40	3 • 39	5.57	5.43	5.113
1115		157-28 169-10 155-38 196-86	155.30	196.86	191.50	154.00	228.10	152.64	145.40	107.00	149.45	215.63	168.00	115.50	3.75	6.19	6.03	5.52
1110	154.24	15%-24 stored larger	Bure her	216.51	215.23	165.80	249.34	175. 14	04.41	182.98	16 1.42	241.50	171.87	115.84	3.97	6.52	6.52	\$ 5
1111	167.60	167.60 239.10 197.10 259.40	127.10	254.441	234.90	219.50	276.60	200.80	1650	111.10	1.0.4	11.6.4	1/0.23	113.50	4 - 33	7.11	1.35	24.49
157	174.60		: 55.00 127.00	21.1.11	26.4.55	16.0643	219.11	2.5.5	174.26	231.10	1.11.1	21.3.4.1	173.10	126.98	4.90	01.1	7.46	6.93
161	1'14.51	282.28	216.34	241.90	251.80	\$10.30	294.9	02.44.45	191.10	255.10	210.50	110.4"	211.40	155.80	3.36	8.50	4.53	1.48
C 11 F	211.40	396.0	25 Tat 1 3. Tak.	5. 7.4.	337.60	310.70	134.11	्रक्ष क केड	25 30	249.60	23)	149.69	263.40	156.30	6 • U6	19.6	2 4 • n	66.39
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APPENDIX E MONTHLY DATA FOR THE HISTORICAL INFLATION PROGRAM

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¥ 2.00	31 - 21 7	10.00	7.50	3,000		282.16	122.70	=	2.15.660	290.90	224.30	379.71	35.	157.00		9.53	9.32	8.31 0]
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1000	94.000			44.0		285-71	\$22.70	= ~	276.60	283.50	250.10	579.70	291.79	163.10			9.62	8.51 30
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7 4 4 7	210.86	123,90		344.21	372.80	71.4	:		224.50	309.80	224-44	377.53	363.50	165.79	5.49 1	10.43 1	11.	
YAMIT	231.90	323.74		349.30	373.50	-7	347.70		25	309.80	22202	377.50	63	165.80			0.25	
71717	233.40	323,33	232 • C :.	368.83	375.50	271.40	372.70	09.	24.50	379.48	550.8	377.53	£6.	167.40	۰.		0.52	9.28 d1
101716	232.16	343.50		368.10	378.76	06.962	372.70	1.6	99	349.kU	75.1.5	377.54	74.	170.20			***	
81416	234.10	343.16		370.00	380.86	121.40	372.70		920	309.80	223.24	377.50	374.80	1 / 0 - 50	.		ກ ເ	
AISEP	235.70	343.50		371.86	383.20	367.10	372.70	5.5	20	309.80	222.40	377.50	74.	170.80	2		رد. د د د	
H10CI	237.50	343.59	235.911	363.69	345.80	292.80	372.70	249.10		309-80	221.70	57.7.53	377.90	170.60			10.01	0 00
512CV	238.91	343.58		375.89	380.90	250.00	372.70	292.50	200		00.812	36.2		7	- 6		101	
310EC		343.90		385.00	395.20	221.40	372.70	2 :		10.00		- 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0	20.11.	174.50	,		6.6	
62 JA'1		543.50		566.7.	37.00	•	312.10			20.40		177.77		175.10	6.3		1.60	0.11 5.
dZFED		37.040		396.98		104 401	473.74		2	308670		377.50	0 20	175.50	6.96 1	_	66*0	3.94 0.
A A B A	2411-011	27.000			70.04		375.75			3 L.M. 2 J.	17.	\$77.53	375	175.69	7.01 1	1.47	16.0	9.99 B.
X 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	24141	5 7 ° F 7 F	0.000			199		0 x 0 x 0 x 0 x 0 x 0 x 0 x 0 x 0 x 0 x		308.70	.)) • "	377.50	75.	175.73	7.05 1	1.66 1	0.6.0	0. U3 E.
146.00		24.24.4			1000	. ~	172	. 1	5	308.10	.01.	377.50	115.	175.60	7.07	1.72	1:11	0.20 H
1000		340.45			399.68	192.90	372.73		٠,	300-10	2.11.5	0 377.59	110.2	175.80	7.19 1	1.74 1	1.20	0.25 b.
A2A15		342.30		415.00	399.60	169.30	312.19	285.44		304.16	2-11-4	311.50	170.2	175.90	7.22 1	1.95	1.28	0.32 8.
9256		3421		415.66		196.40	372.70	7 h 46	224.00	300.00	207.16	377.50	370.20	176.40	7.2H 1	2.00.1	1.30	0.41 A.

APPENDIX F HISTORICAL INFLATION INDICES

	AIRFKAME	REKAME PRINCELION	ENGINE	ENGINE PRODUCTION	AG. BLSATE EXCLUDING	AG, REWATE AIR VEHICLE Excluding avionics
	INCEX	FACTOR	Inofx	FACTOR	10 mm 20 mm	FACIOR
	CYb7=	F Y 82=	C167=	FYB2=	101.	- 2014
	136.1	1.000	1,000	1.0000	0 • n t; 1	1.0000
; ;			:		! ! !	1
7	17.3	6.8432	5.53	5.9059	49.1	6.6128
<i>?</i>	52.1	6.225#	61.A	5.2763	5405	5.9949
6.1	53.0	6.421.	53.1	5.1646	6.04	5.4149
r.s	55 4 • 5	5.7150	6.4	4.9106	9.8€	5,5121
75	62.4	5,1921	73.3	4.4455	6 • 40	5.045
\$2	64.7	5.0114	74.9	4.3524	b 7 • 0	4.8477
3.3	61.5	4 . 6 1168	17.8	4.1877	49.B	4.6533
i.	4.69	4.6796	75.3	4.1084	11.6	4.5322
50	73.1	4.4335	0.49	3.8792	15.6	4.2965
96	17.6	4.1761	90.2	3.6132	4.02	4.0573
57	79.5	\$ 698¢	45.5	3,5238	82.7	3.9263

						ALGRESALE	AIR VEHICLE	*************************************	AIR VENICE
AIRFRAML	AIRFRAME PRODUCTION	30105.1	PRODUCTION	AVIONICS	PRODUCT10N	F XCL UU ING	AVICUICS	INCLUDING	AVIONICS
INDEA	F 4C T JA	It. UEX	FACTOR	INDEX	FACTOR	I EOE A	FACTOR	I Mee x	FACTOR
C 767=	FY82=	CY67=	FYBZ=	CY67=	FY82=	CY6/2	F Y 82 =	CY67=	F Y 42 =
100.0	1.0000	100.0	1.0000	100.0	1.0000	100.0	1.6000	1 5 0 • N	1.0000
!	-	!	1 1 1 1 1		1 1 1 1 1	1		* 1 1 1 1 1	! ! ! !
F2.4	3.9311	94.2	3.46.39	H. C.	3.1916	35.4	3.8159	44.7	3.7566
63.1	3.0932	32.n	3.0161	83.2	3.1281	₩5.4	5.0.23	85.1	5.7569
65.2	3.8420	95.5	3.4117	85.4	3.0465	9.18	3.7974	87.5	3.6428
96.0	5.7712	45.6	3.4972	87.4	2.9751	188.1	3.6834	88.1	3.6131
87.1	3.7209	40.0	3.3994	86.1	2.9516	89.1	3.6440	69.0	3.5754
r. 6. 9. 7	3.6823	4.46	3.4521	i•68	2.9232	44.5	3.6287	4.68	3.5565
89.2	3.6303	52.3	3.5503	91.1	2.8541	6.48	3.6113	u•u6	3.5347
92.3	3.5119	92.7	3.5149	92.ú	2.8090	92.4	3.5125	92.4	3.4421
96.5	3.3609	75.5	3.4128	95.5	2.1246	96.3	3.3723	2.96	3.3080
100.0	3.2424	1.0.0	3.2590	100.0	2.6012	10.0.0	3.2461	100.0	3.1816
103.8	3.1236	164.6	3.1156	1.4.1	2.497₺	194.0	3.1218	104.0	3.0593
110.4	2.9375	1111.1	2.9322	106.1	2.4057	114.6	2.9363	110.3	2.8843
116.9	2.1745	121.8	2.6754	113.2	2.2980	110.0	2.7518	117.5	2.7031
120.9	2.6639	127.6	2.5544	117.4	2.2149	122.3	2.6532	121.9	2.6109
128.5	2.5151	130.7	2.4928	121.0	2.1542	129.3	2.5100	128.5	2.4762
1.17.7	2.3538	135.3	2.4395	125.4	2.0745	137.2	2.3663	136.0	2.3591
154.0	2.1056	157.2	2.0734	134.3	1.9364	154.1	5960.5	152.7	2.0841
172.0	1.8851	178.1	1.9296	146.2	1.17.1	175.4	1-672+	170.6	1.5545
1:4.6	1.756t	169.5	1.7165	152.7	1.7635	185.K	1.7475	182.5	1.7438
197.E	1.6365	207.7	1.5688	164.4	1.5825	200.0	1.6227	196.5	1.6153
214.8	1.50%	219.4	1.4856	163.4	1.4182	215.8	1.5042	212.6	1.4967
237.6	1.3645	246.7	1.3246	199.1	1.3027	244.5	1.3554	235.5	1.3509
271.3	1.1952	294.2	1.6494	226.0	1.14/0	21115	1.1693	212.4	1.1500
364.7	1.6643	314.9	1.1349	246.7	1.0542	\$00.9	1.0576	300.9	1.0575

 $\label{eq:condition} \Sigma = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} = \{ \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} \} = \{ \{ \{ \{ \}_{i=1}^n \} \} \} = \{ \{ \{ \{ \}_{i=1}^n \} \} \} = \{ \{ \{ \{ \}_{i=1}^n \} \} \} = \{ \{ \{ \{ \}_{i=1}^n \} \} \} \} = \{ \{ \{ \{ \}_{i=1}^n \} \} \} = \{ \{ \{ \{ \}_{i=1}^n \} \} \} = \{ \{ \{ \{ \}_{i=1}^n \} \} \} = \{ \{ \{ \{ \}_{i=1}^n \} \} \} = \{ \{ \{ \{ \}_{i=1}^n \} \} \} = \{ \{ \{ \}_{i=1}^n \} \} \} = \{ \{ \{ \{ \}_{i=1}^n \} \} \} = \{ \{ \{ \{ \}_{i=1}^n \} \} \} = \{ \{ \{ \{ \}_{i=1}^n \} \} \} = \{ \{ \{ \{ \}_{i=1}^n \} \} \} = \{ \{ \{ \}_{i=1}^n \} \} = \{ \{ \{ \}_i \} \} = \{ \{ \{ \{ \}_i \} \} = \{ \{ \{ \}$

		4	IRFRAME	PRUBUCT 10N	ENGINE	FRODUCTION	AVITHES	PRODUCTION	ASCRESATE EXCLUSTNG	AIP VEHICLE Aviouiss	ASGREGATE INCLUDING	AIR VEHICLE Avionics
		-	130£ X	FACTOR	I NDEX	FACTOR	1401	FACTOR	1 c x	-	INDEX	FACTOR
		ı	Y67=	FY82=		F Y + 2=	CYE7=	F182=	CY t- 7=	Ţ	CY67=	FY82=
		~	36.4	1.0000	10 :00	1. 10:00	160.	1.634	l. , . l	1.6333	160.4	1.0039
!		•	1	:		• • • • • •			1 1 1			!
J:L		IJ,	99.3	~	3 0 11 11	5.2173	136.5	•	6.66	208		•19
Ato	~	1 00					100.2	.596	144.3	-2		.173
SEP	~		Ξ	3.2211	100	~	٠	េះ	٠	.226		.164
100	~	_	_	~	2	.13	-	. 585	101.4	* 2.		141
A OR		_	02.1	-	102.1	_	000	5	102.1	.17	132.0	.119
050	~	_	0.5	7	103.2	861.	142.0	ຳ	102.9	3.1552		. 1195
440	T)		20	7		.14	102.5	5	102.7	• 16		.098
FIB	Ŧ	_	02	7		.13	103.3	5	142.0	3.1565	102.9	.032
346			2	3.1605	1.13.8	-	103.2		1 112 . 9	3.1553	102.9	3.4920
47.4	œ	-	01.	7	•	٦.	02.	.5	142.1	~	102.2	115
741	æ	_	02.	-	104.1	13	03	5	102.8	ç.	102.8	.93
200	æ	_	02.	7	104.4	7	104.1	4	103.1	3.1471	103.2	160.
J1F	7.		02.	7	104.5	-	4.	7.	1.13.2	÷	3.	.081
Auō	10	-	63	7	105.2	•	4	4	16.4.1	3.1168		. 153
	m		. 40	e	1.15.3	•		*	104.9	3.0951	104.4	.033
	70	_	1,6	•	1,5.6	•	Š	*	190.4	3.0519	106.3	.934
	ю		07.	<u>-</u>	6.0	3.0789	105.9	3.	1.66.1	٠.	106.5	583
	20	. 63	٦.	7	107.1	•		•	101.5	_	107.2	996.
	•		07.	٦.	۳	3.0153	٠	٠.	1.17.6	٠,	107.5	966
		. 69	8	2	L	•	107.4	*	: 113. ft	2.9345	•	928
	c	-	8	٠,	1.8.1	=	167.2	3.	1.9.1	•	168.6	.930
	,	1 69	9.	e.	166.4	0.0	106.9	4	1:4:1	3.	å	.922
	Ŧ	59 1	ċ	2.	149.0	64.	107.8	3.	103.2	٠,		.917
	7		ę.	6.	116.3	. 95	108.1	2.4064	1.19.6	5	6	.907
Jer			60	٠,	113.6	46.	108.4	•	109.6	ς.	6	•906
9n*			11.	٠.	•	3	108.1	•	~	5	ċ	.871
SEP	6		Ξ	•	•	7.	1601	•	=	5	ċ	.881
100	•	-	~	8	115.5	٠	6	•	~	.872	5	. 82
۸C.	4	-]	8	115.4	æ		•	*	.844	÷	• 13
0.0			=	ı.	115.4	~		٠.	_	8.	115.1	• 16
N.4.0	_	-	;	<u>ء</u>	120.4	٠,	=	. 343	·C	146.	ŝ	٠75
ลา.		_	5.	٤.	120.4	٦.	110.9	•	110.2		115.7	• 75
244	e	_	5	÷	120.7	٦.	=	•	116.3		115.8	٠7،
* 1	ح	_		٩	100.7		111.3	2.3245	110.6		116.1	.74
1 t Y	_	_	15.	Ŧ,	101.1	2.8514	112.5	٠	11:09	2.7764	116.5	. 7.3
せつつ	-	_	15.	• 19	121.0	2.0016	113.	•	11/.1		116.4	. 12
111	ي	_	7	. 15	121.	2.67:5	114.1		-		117.0	
ALC.	٠,	~	, 8.	. 7.	3.5.5	2.000	114.4	•	118.4	17.9	114.	• to 8 t
125	٠.	_	30	.12	1.2.4	2.6624	114.3	2.26.56	11 1.6	.715	119.2	.670
100	-	-	15.	2 • 72-:	128.9	2.64.04	115.1	٠,	119.4	•	119.4	ę.
*CN	1 :1	1 1	20.5	•	125.0	2.136	110.7	* 2.4	1.11.1	^ 1	123.	40
ن و ر		~	24.	•	1.4.9	2.60.3	116.7	5.0.93	171.3	2.6750	126. ?	2.6.52%

			JIRFKAME	IRFRAME PHUGUCIION	Eusthe P	FROUDCTION	AVIONICS	Teales traducation	40 RESATE LYCLUSITE	the violity	46667 5416 14CL 00145	AIR VEHICLE Aviumics
			X 30 EX	FACTOR	c	FACTOR	11:01 X		N John H	FACTOR	INUEX	FACTOR
			7	Y 62 =	CY67=	- ∿1	CYe7=	FY 82=	CY:7=	FY82=	CY67=	>
	ر ح	>		5	-	~	106.0	ij	•	Ē	1001	
	:	;	:::::::::::::::::::::::::::::::::::::::	1	1		•	1	•			-
1,40	1.1	7	119.)	~	124.7	2.61.25	117.3	.21	121.0	2.6832	ė	• 65
		7.	6	. 111	9	3600	117.1	3	124.8	2.6467	÷	.641
	7.1	11	g.	.747	25.	.591	117.E	.21	1.11.1	2.6805	ė	635
a T	7.1	1	Ç,	. 702	25.	•590	111.7	.217	121.3	2.6764		631
	7.1	7	121.2	2.6750	40.	5.7 E	117.8	2.2070	122.3	2.6532	•	ø
	7.1	7.	3	.680	æ	2.5365	m.H.	.200	122.4	2.6517	~	637
		72	120.0	.6 8₺	28.	.531	3	2.2052	122.4	2.6521	?	.608
	7.1	12	121.2	. £ 7 is	200	•528	1 B.	2.2046	122.9	2.6417	٠	. 599
S.P	7.1	72	121.6	3.7	128.6	.531	118.2	2.2015	123.2	2.6348	ċ	•
	7.1	25	122.1	.656	29.	.522	17.	2.2236	123.5	2.6253	÷	•
	7.1	12	122.7	.642	29.	3	17.	2.2192	124.2	2,6133	•	2.5759
	7.1	12	123.2	.b31	30.	664.	18	2.1970	124.8	2.6008	÷	•
	12	12	122.f	.644	•	* b C •	118.9	2.1676	124.3	2.6114	÷	•
	72	72	125.e	.581	31.	. 4 B B	119.2	2.1818	126.8	2.5630	٤	•
	12	72	126.h	•55e	5:	111.	120.1	2.1659	127.9	2.5387		•
	12	72	128.b	.517	151.7	.473	119.1	2.1723	124.4	2.5080	å	•
	12	72	128.c	.521	32.	. 45B	120.6	2.157	123.5	2.5009	å	. 47
	72	7.2	128.6	.521	28.	.543	121.1	2.1474	128.5	2,5263	•	5-4904
	12	7.3	127.1	.551	24.	.535	121.5	2.1416	127.4	2.5481	ġ	.50
ور	7.2	73	129.6	. 501	128.6	٤,	121.4	2.1433	1.29.4	2.5489	128.6	•
	12	73	130.2	.491	129.0	. 525	122.1	2.1501	121.9	2.4987		.463
	13	13	3	.475	129.3	.524	122.1	2.17.06	150.6	2.4850		•
	12	13	~)	• 429	1,49.1	.511	121.6	2-1554	132.7	2.4462	<u>.</u>	4
	12	~	134.9	* 7 % •	131.6	.477	123.0	2.1143	134.1	2.4200	×,	~
	<u> </u>	73	134.1	~ ~	1 50.9	9.4	15:01	2,1113	1 55.4	2.4341	ċ	2.4143
	7.3	13	٠	. 4 i	131.0		122.0	2-1105	134.0	50050	132.9	2.3943
		7.1	135.3	. 59c	132.6	4.5	***	2.1077	124.7	2.4094	÷	2.381r
A F R	7.5	7.3	135.3	395	132.7	4	124.1	2 • 0 • 2	7 * * * 7	2.4096	÷	2.3865
	2	7.3	•	~	134.2	. 4.	174.5	•	137.6	2,390	134.1	2.562H
	7.5	~ ?	•	٠,	135.	•	124.5	2.0830	1 40.5	2. 53 5b	1.55.0	2.5564
	7.5	7.		175.	156.03	165.	125.2	,		2.3825	135.1	2.3544
	7.3	ž	œ	. 547	136.5	. 387	126.7	٠.	1.4.1	2.3000	136.7	2 • 32 + 2
	13	<u>.</u>	1:4.1	. 336	•	•	12i sń	2.0543		2.3415	137.4	2.5150
	7.5	7.	1+1-1	• 290	•	•	1.7.	ξ.	144.5	2.3140	÷	2.2849
>	7.3	* /		, . T	134.5	•	1.7.1	2	·	2. 10.50	139.0	7.2741
G	~	7.4	143.0	۲۶,	14:00	•	1,24.1	<u>-</u>	•	2.2714	141.5	2.2442
2	1.4	1+	3.561	N	1:1.4	•	1.4.4	Ξ	145.6	2.26.91	3	~ `
Z)	* ~	*	2.404.	55	141.4	•	15.3	2•44P1		2.5403	•	-
I T	*	7.4	1470.	¥	145.4	•	130.4	1.93.2	7.00	8512.5	4	The second
▲	*	<i>z</i>		91	144.5	•	1.51 •	1.9855	147.6	2.2953	145.0	S
171	5	<i>-</i>		-	1.4.1	٠١١,	 		~ ·	2.15.7	٠,	-:
ار الاراز	± ,	₹.	156.5	7.1255	3 ·	10/10°	· • • ·	; ;	· ·		151.4	2.1119
1	5	<u>.</u>	٠	=	J (: • L)	2.48.4.5	1 5	\ ~	Z • 7.0.	2.045.	-	=

HISTOPICAL ILFLATION MOLINEY INDICES

		ন	IRFKANE	IRFHANE PRODUCTION	Englnf P	PHOFUCTION	AVI JEIC	FROUCTION	AcontoAT: EXCLOSING	AIR VEHICLE AVIONICS	AGUELCATE INCLUDING	ATE VEHICLE Aviorics
		Ξ	-	SACTOR S	1000	FACTOR	4 1001	FACTOR	N II I	FACTOM	INDEX	FACTOR
		i (× 5.7 = ×	, ,	(16.7	FYRDE	C 7 L 7 -		61.17	FYBJ=	CY n 7 =	F Y 82=
•	_	- ر	5	٠ -	20.7	ייי"ן	, t. n. (1.000	1 10 . 0	1.6590	1.30.0	1.000)
		٠,	: ;							1 1 1 1 1 1	!	:
7119	7.	36 10	~	1.6.1	166.1	961	155.4	1.9210	15.9.5	2.0377	155.9	•
	. ,	-	1		167.0	1.0513	137.3	1.8950	100.3	2 • 02 4 3	155.0	2.013/
		-	-		168.6	1.9331	137.6	1.890c	162.9	1.5926	150.4	1.5834
		-	٠ ۸	. 6	169.3	1.9246	139.4	1.8692	164.2	11	161.7	1.9671
		-	,	5	171.8	1.4974	141.9	1.8325	105.3	1.9634	163.	1.9521
		-	ċ	96	177.3	1.8581	143.2	1.8163	169.2	1086-1	1 65.7	1.9202
FEB	0	. ~		95	176.1	1.6515	144.1	1.8054	30	1.9297	165.4	1.9130
	חו	_		93	176.7	445	144.5	1.8007	169.4	1.9164	166.3	1.9064
	יט	_	2	.91	177.	1.8413	145.2	1.7910	170.7	1.9417	168.1	1.6921
	0	_		.902	116.4	33	145.6	1.7865	172.2	1.8649	169.6	1.8765
	··c		-	.885	177.5	1.8369	146.8	1.7718	175.2	1.6744	170.5	1.8656
	٠.	-	2	.57c	177.9	1.8366	~	1.7582	173.7	1.8598	171.1	1.8592
	חיי		74.2	1.8605	174.1	1.8296	÷	1.7706	175.1	1.8538	172.3	1.8467
	un.	_	75.1	1.8515	179.1	1.4193	147.6	1.7623	176.0	1.8442	175.2	1.8373
		-	76.3	1.8374	179.5	1.6159	147.4	1.7646	177.C	1.8341	174.0	1.8282
			77.8	1.8235	179.1	1.8197	147.5	1.7631	178.1	1.8226	175.0	1.8176
		_	78.7		181.6	1.7947	148.7	1.7492	179.5	1.6105	176.2	1.8052
	ı w	_		1.6104	185.0	1.7615	149.1	1.7382	100.4	1.7393	177.3	1.7941
	<u>ت</u>	_	B		185.5	1.7592	149.5	1.74.11	181.7	1.7855	176.5	1.7826
	9	-	d1.0	1.7854	165.	1.7493	149.8	1.736.4	132.3	1.77.1	179.5	1.7724
		_	81.2	1.7850	134.4	1.707+	149.9	1.730	181.9	1.7546	174.7	1.7805
	9	_	42.5	1.7731	156.6	1.7468	150.8	1.7252	153.7	1.7072	180.4	1.7637
AUC	نف	_	b3.6	1.7720	107.3	1.7401	151.8	1.7134	1.55	1.7648	180.7	1.7605
JIL	9	-	80	•	190.0	1.7150	152 • 8	1.7028	186.6	462L*T	183.2	1.7363
4.15		_	85.	1.746"	192.0	6.63.1	153.3	1.6967	147.5	1.7332	133.4	1.7302
	vo.	-	Rt 3	•	194.0	1.6748	1,74.1	1.683	144.5	1.7225	1 45. 1	1,7195
	9	_	: • 6 H	1.7140	104.1	1.0/4.1	155.1	1.6774	****	1.7050	186.9	1.702/
	9	_	1.59	•	1.15.3	1.00 BS	155.7	1.6719	191.0	1.6997	187.4	1.6973
0.53	w	_	40.0	1.701	1)6.7	1.056.6	158.7	10 to 10 to	6°11.1	1.6911	3 3 4 · 1	1.5 2 6 7
Jin	_	_	91.6	1.69	198 et	1140.1	۲۰۵۶۱	1.624.4	115.2	1.6334	183.4	1.6/33
	~	_	92.3	•	173.8	1.0337	166.1	1.5862	0.54	1.67.5	194.	1.6642
	~	_		•	232.1	1.6" 75	166.2	1.52 16	L+2+1	1.6004	1 42.	1.55/3
A	_	_	95.1	1.6.6%	242.1	1.0077	161.0	1. blos	1 17.0	1.4.4.	193.4	1.6455
	_	_	95.7		20004	1.47.42	162.1	1.6044	195.4	1.0525	19%.2	1.0507
	_	_	77.4	1.6.4.76	20000	1.5-5	163.9	H T	1.4%.0	1.6242	196.	1.6710
	~	_	5 H.	1.6201	210.2	1.5248	154.7	16/401	*• I ·	1.0115	197.8	1.6'.8H
	7	`	2.90	1.6174	216.5	1.5494	167.	1 7 -1 4		1.6.155	194.	1.6.133
	۲-	e.	01.5	, 11 ; 1	211.4	1.42.6	16.7.3	04.64.	4.500	\$565 *1	÷	1.591:
	_	~	Ē,	1.61.	212.1	1.77.	172.	1.5104	2 n 7 • 4	1.5 5.1	2.10.3	5
	_	٠,	÷	1 5.5 7.0 1	217.0	1036.1	175.1	1.5011		REFG-1	Ξ	1.5767
		: "		1. 5. 7	21.00		175.	1.4830	1.1.	1.6749	203.1	1.5669
346	r	٠,	0	1.7.7.1	215.1	1.7.105	11.0.3	1.4.7.4	2010	1.500.1	1.4.1	1.5585
534		• •	٠		10313	* (T) * T	174.1		, t	1.051	7.0c.	1.44.3

		AIRFAARE	F 8 DUCT 104	ENGIN	PRUGUETICA	AVISTICS	PRUDUCT13B	AG JREGATE EXCEUDING	AIR VEHICLE Avionics	Ağgri gate Inci uğing	AIR VEHICLE Avionics
		INCEX	A.C.	1.06 x	•	NOE'S	<u>-</u>	:	A C F	NDE	_
		.Y67=	F Y 52=	CY67=	F Y 8.2 =	CY67=	¥82	CY 5/2	Y82=	CY6/=	Y 8 2 =
ر		100	-:	1.49.0	-	100.1	1.11718	_	5.33	Š	.00.
			::::	1		;	-	1	;	•	:
~			1.556.0	514.2	1.4.	:t	***	7	•	206.7	S, I
*			•	214.1	7 - 1	174.7	**	<u>:</u>	1.5391	=	so.
-			1.5397	215.2	1.31	180.	\$	Ξ.	1.533	~	an ı
			3,	217.6	1.41	181.6	1.4322	12.	1.5256	209.7	(1)
			1.5187	220.1	1.40		.*1	÷	1.51 12	_	1.5024
			.4.	221.7	1.45		J	211.66	3	-	1.4651
			1.4918	223.2	-		. 395	~	4554	-	1.4769
			-3	22.3.5	-	ăÉ.	C.	~	* 34.	_	1.4589
			•	223.1		4	. 384	223.5	1.45.23	cu.	1.4405
			*	228.5	-	51.	•	ζ.	.437	~ .	₹ .
			•	228.4	-	•	•	$\tilde{}$. 425	O.	1.4192
			1.4229	229.7	-	192.1	•	20	*	~	4
			1.4163	231.5	-	6	-	3	415	~ .	4
			1.4112	235.8	-	93.	1 - 344 7	5	٠.	O.	1.4320
			1.3898	241.3	-	•	•		386	~>	~
			8	245.1	_	97.	•	5.	~	₩.	•
			1.3578	245.3	-	96	1.3050	7	. 353	~	σ,
			.362	251.4	-	91.	•	241.0	. 546	•	•
			.351	253.4	-	*	.273	245+3	3.55	•	,
				217.2	~	15.	٠	251.1	6 ac.	₹.	Σ •
			•	232.2	1.1.47	207.1		20°	1.2544	റം	0,
			1.2740	24.7.1	1 - 1 3 5 2	2	٠	်ပါ•င်း ၁	ຕ	n.	• •
.14P. C	6.9 8.0	1 25cos	7	20405	1.1469	215.3	5×500 € T	្រ ប្រ	n (201.0	4.000
			?	= (1690-1	<u>`</u> :	7 -	2.07	710701	0 4	1 2 4 4 5
			20.0	٠.	20.60	: :	•	0.0	0.61-1	0 4	4
				3 8	721101	7	11.17	,	1 1 2 7 9	3 (2447
			1.2154	2.44.5	- an I - I				1.1795	3 ~	1.1759
200				, ,	1 26 1 16	<u>ئ</u> ر د	•	21.72	1.1668	. ~	1.1644
				25.4.9	10000	2	1.1501	24.0.5	•	_	1.154)
			1.1740	-	*450	3	1.1263	201.4	1.1557	_	1.1569
			1.1542	299.7	20	3.5	1.1166	S.	1.1385	~	=
			1.1354	36.1.4	1.1411	34.	1.1076	7	1.1222	30	1.1213
			1.761	\$ 10 C . 4	-	31.	1.0473		•	Œ	Ξ
			-	-	1.16.75	7	1.4851	2.15.3	•	244.4	n 3
		~	1.1070	50018	1.401.1	<u>.</u>	10.11.4	7.4.7	•	90.	1.0962
	_	366	1 • 0 %	2020	1.4.2.1	7.4.1	-	# • 1 c.	1.300	5	
	_	7	1. (2)	\$14.2	* · · · ·	,	1 / 4 1		<u></u>		1.0367
	_	(1)	1.07.5		1.04 32		<u>-</u> ا	5.45.	U / U	241.	7 (
	-	, 6,	1.1.	÷	· · · · · · · · · · · · · · · · · · ·	7.47	1.6.1.4	٥.,	1. 1.00 - 1	6.6	1.0.54
			1	511.11	• • • • • •	· · · · · ·	Ţ	C • / : .	Ē	10101	1. 126.6
	<u> </u>	÷	3 5 6	21 m	-	=	<u>-</u>		1.740.1	3.7%	* * * * * * * * * * * * * * * * * * * *
	_	1 5 194 .	10147	413.1	1.1.1		1.11.	511.7	- U * U * I	50%	

			AIRFRANE	AIRFRANE PRODUCTION	ENGINE	PRODUCTICA	AVICTICS	VICTICS PREDUCTION	AUTHENATE EXCLUDING	AIR VEHICLE Aviorics	AGGE! GATE Including	AIR VEHICLE Avionics
			INDEX	AC I	1.06 x	FACTOR	1806.8	13	17.00 X	4 C I	NDC	FACTOR
			CY67=	F 1 82=	CY67=	FYB.?=	CY67=	F Y 82 =	CY:12	FY82=	CY67=	¥82=
	ځ	FY	100.	O	1.49.0	1.6409	106.1	1.11990	141.3	~	÷	.00.
;	;	;	:		:		!		:	1	;	;
X 2 R	£.	76	206.4	555	514.2	1.5215	179.6	1.44487	2 19.7	1.5481	206.7	S
A 7.	7 85	7.0	210.3	1.5443	*	1.5223	174.7	1.4476	210.9	1.5391	=	531
4 7 A	7.3	7.8	216.6	5	'n	1.0141	180.	~	211.6	1.5539	JH.	52E
77	₹	76	211.4	63.83	217.6	4	_	1.4322	212.H	רט	. 4.0	2
176	Ş	74	5.515	.5163	220.1	409	163.	1.4125	514.5	1.5132	.:	1.5024
400	73	16	216.4	.4382	221.7	944.	194.0	1.4135	217.6	1.4918	14.	4
SEF	£ (76	217.3	916	223.2	4	186.4	1 • 3952	218.6	1.4847	15.	476
100	78	44	221.1	.4604	223.5	•	186.8	ð	221.6	J	H.	58
ACI.	7	Ď.	223.€	.4584	223.2		167.9		223.5	1.4523	0	3
) <u>:</u> C	£-	7.9	225.1	*****	224.5	•	191.1	36	225.9	1.4372	22.	430
242	19	19	227.5		228.4	•	191.5	S	271.8	1.4250	24.	19
Ti I.I	5.	7.2	227.9	.4229	229.7	•	92	350	228.3	1.4219	24.	1.4158
HAR.	19	15	228.É	.4163	231.5	•	m)		229.3	1.4159	25	1.4100
AFR	7	19	229.8		233.8	1.3941	~	1.3447	250.6	1.4074	56	1.4320
TA1	13	61	233.3	.3896	241.3	.350	•			1,3809	3	1.3771
NOT	49	61	234.2		245.1	.329	~	31	Sa.	1.3724	32	67
اباد	13	7	237.3	1.3578		•	199.3		3	1,3539	3.5	349
AUG	73	15	23h.1	1.3620	-	1.2964	201.4	1.2924	241.0	1.5468	3.1	342
SCF	61	51	240.6	1.351.	253.4	1.2855	2114.3	1.2734	2+5-0	1.3359	39	30
120	2	7.5	240.0	1.3192	ž	_	205.1	ć	251.1	Cu	7	T.
ACT:	13	Ċ	252.1	1.28: 3	232.2	1.1347	207.1	552	258.8	1.2544	253.6	1.2543
0.0	13	ນ	中 中 中 的 C	1.2740	20.7.1	.135	212.5	554	3r]•b	S	56	ν. Σ
.J.A.P.	6.9	B 0	25e - 3	1.26'2	204.2	. 14t	215.4	202	G*747	2	2.	34
7 F.	g E	G E	258.7	1.253	31:05	1.497	217.6	35	.0/	1.2013	265.0	9
148	e. T		259.7	1.2444	312.5	1.5428	214.8	1.1637		1.1928	99	1.1948
۲ ۲	B n	÷	265.0	1.2753	535.9	1.1127	221.9	1.1722	2110	1.1309	:	1.1948
1 A Y	E	Ç	20105	1.2134	94.	1.1067	C-4	?	-	1.1879		1.1462
Š	3	G G	269.4	5	95.	1.1025	್ಟ	_	•	1.1795	_	1.1769
71	Ę.	3. 1.	272.E	.18	2+1.2	96.			218.2	1.1668	273.2	1.1644
A 15	σ.	r	275.	.174	25.4.9	1.6460		1.1501		1.1572	•	1.1543
3. W	į	ب	276.4	. 17	-	1.0304	~	~	<u>-</u>	1.1537	76.	1.1569
100	C	81	580.5	un.	299.1	1.0873	~	116	٠ بر	€	÷	1.1367
, c.	ьĵ	£ 3	285.1	1.1354	Ĺ.	1.1411	234.H	1 :) 7		C1	285.7	1.1213
၁ <u>၂</u>	(₹	247.4	1.1260	3110.4	1.171.	£3£•9	1.0479	=	Ξ	ŗ	1.1148
7.7	.	<u>.</u>	3.06€	1.116	F + 7 E 5	1.16.75	233.5	1.4461	213.2	7.1.4	ĦĦ.	1.1033
2) •	-	.,	292.1	1.1070	5000	1 . 1042	1-143	1.07.13	2.4%	1.0978	=	1.1962
342	Ę.	Ξ	7.00	1 • 0 5	だっていい	7.57.2	1	1.1745	\$ • 3 · 6.	1.906.1	2	1.0451
AFR	<u>-</u>	7	1.15	, . , , . • [510.0	4	1.0	1 • / 4 1	C • 6 to 1	1.01.	794.4	1.0867
¥ 4 ×	.	7:	5.13.	1.97		1.0030		1.00.7	20.5	2	297.5	776
2	÷	-	102.5	1.01.	2 1 + 1 °	1	547.4	1.6.7.14	٠٠٠	1.00.1		1.3754
1,	-	,	* * * 7 : "	1.00	514.1	1	S * 7 *.	-	6.11.1	1.6574	191.1	1. 15th
9.4	ī	- :		1.41.	F = 12 TV	1.00	1 . 110.	1.63.7		Ę	395.5	1.14.1
÷:0	-	-	5 19	1 * 1 4 7 .	117.1	11.	# C + 1	1.871	5111.7	1.041.	\$044.0	1.041.

4 July 1

			AIRFPAME	Production	EUG INE	PRJOUCTIUM	AVIONICS	PRODUCTION	AUGREGATE EXCLUDING	AIR VEHICLE Aviorics	AGSHT GATE INCLUDING	AIR VEHICLE Aviorics
			INDEX	FACTOR	INCEX	FACTOR	INDEX	FACTOR	1 i. ii E X	FACTOR	INDEX	FACTOR
			CY67=	FYB2=	CY67=	FY 02 =	CY67=	FY 82=	CY57=	FY82=	CY67=	F Y 82=
	Č	FY	100.	1.0000	136.	1. 100	100.6	1.00.1	160	1.0440	100.0	1.3000
;	;	;			1 1 1							
120	T.	8	315.2	1.6284	322.3	1.3112	251.1	1.0362	515.H	1.0248	310.2	1.0257
* C <	£ 3	2	317.6	1.02.3	325.6	1.0166	252.1	1.6324	318.4	1.6195	311.8	1.0205
3 i c	E 3	ı.	321.5	1.00.14	375.6	1.4927	255.1	1,0197	522.1	1.0079	315.4	1.3089
345	c.	4	422.9	1.0041	325.7	1.0369	259.6	1.0029	\$23.1	1.0047	316.7	1.0.145
EI Lu Lu	Ç,	3.5	324.2	1.01.7	323.7	1 130	258.3	1.0074	324.5	1.0:102	317.9	1.008
346	71	82	323.5	1.0018	325.2	1.6922	259.6	1.0020	324.0	1.0019	317.0	1.0019
AFR	6.2	42	322.7	1.0048	326.3	0.9349	266.5	0.9945	323.5	1.0035	317.2	1.0431
TAF	C)	82	525.4	6.9955	325.7	1.3005	261.7	0.9939	125.5	0.9974	319.1	0.9971
.00	42	2	22701	3166.0	327.4	4566.0	262.3	0.9918	527.1	0.9923	320.6	0.9923
115	7,	۲ ×	327.5	1:55.0	329.0	6,49,15	265.9	9784	3.7.7	4066-0	321.5	3.9896
1116	Ą	Ţ.	331.2	U.9791	330.0	0.9875	266.8	0.9751	330.9	0.9810	324.5	9.9805
30.00	~		112.4	44,66	329.9	0.9879	266.7	0.9681	331.8	0.9782	325.5	9774

									•		
		AIRFRAPE	IRFRAME PRODUCTION	ENGINE	PRUDUCTION	AVIONICS	FROOUCTION	ACGRESATE EXCLUDING	AIR VEHICLE Aviouics	AGGR: GATE Including	AIR VEHICLE Avidates
		1 NOE x	-	1 white x	FACTOR	INCEX	2	1 SUPEX	A	104	ACT
		CY67=	FY62=	C107=	F Y 50 =	CY57=	F Y A2=	CY67=	82	79	
81.7	⊁ .	100.0	3	Ţ	č	1 U.C. A	.00	<u>=</u>	. n u		. 300
:	:	1	1 1 1 1 1	1	1 1 1 1	:		1 1	:	;	
	£ 7	160.1	.239	5.66	97.	100.3	59	;	\sim	÷	.176
3	:1	162.6	.17E	CI	11	:	.570	؞ؙ	.17	5	.
·•	<u>بر</u> ۲.	162.5	•16¢	P3	3.1421	105.0	. 524	\sim	• 15	162.9	• 03
	60		·167	13	.139	*	• 1 c •	٠,	10	132.5	969
	Ŧ.	103.0	-	ę,	-	104.	.487	1.4.1	=	•	. 055
	· q		.031	3	Ξ.		459	106.8	• 03	106.7	6.
	£ 3	•	.590	8	7	100.9	•433	•	•66•	ŝ	. 94.
	£.		167	109.2	2.9833	~	.417	169.3	.97	109.1	16
	59	110.3	946.	$\overline{}$	τ,	÷	.390	1.3.	\$ 7.	10.	88
	5.	113.6	.855	9	٠,	è.	.370	7	* #	13.	. 195
	7.0	15	.613	120.5	٦.	_	. 340	16.	• 19	15	. 149
	7.0	115.7	. 803	_	٠	å	.338	16.	. 17	٠	.732
	7.3	17.	. 75£	~	5	<u>:</u>	.273	18.	. 73	æ	1691
	9.			~	2.6321	115.9	٠,	5.0	.648	•	64
	11	119.4	.747	S	9	17.	2.2171	21.	.683	_	.638
	7.1	120.6	• 6 E t.	æ	¥:	•	۲,	5	.669	_	•616
	7.1	21.	119.	126.8	3	<u>.</u> 6	2,	22.	*7•	S	.600
	7.1	22.	*4.	1.651		7.	.21	24.	.613	~?	•575
	7.5	25.	ċ	130.9	*	•	. 17	26.	• 56	L)	.532
	12	•	.521	130.6	*	•	• 15	·	.513	20	. 48.
	12	Ş	•	N	37	121.5	•	168.9	15.	128.2	482
	25	•	435	::	3	ζ,	-15	132.5	• 450	-	• 45
	13	134.8	.490	1:1.5	٠,	125.1	Ξ		.422	132.9	۳.
	2	156.3	.364	134.1	*	•	. 0.5	135.6	.394	4	•
	33	33	.351	36	¥.	125.9	.065	137.7	.308	•	7
	73		.261	1.88.7	W)	128.1	•	•	.236	C	Ç
	*	•	.222	7	٠,	129.0	7:17	145.0	.238	143.5	Ç
	74	151.5	_	•	-	ς.	•	•	• 15	C	•
	*	56.	• 06L	3	Ţ,	156.	2	Ť.	. 948	156.2	-
	*	•	995	169.9	1.9182	1 59 · d	.800	;	.911	•	1.9670
	٠ <u>٠</u>	•	646.	176.7	*	143.4	~	•	• 925	•	<u></u>
		•	•	117.6	1.8347	145.3	•	٠,	. 88	ċ	78
	75	7	•	~	1.5245	-	. 763	•	. 65	172.2	4 7
	3.	177.0	۲,	2	1.160	147.9	16.9	٠	^	•	3 2
	91	180.5	•	165.5	1.1306	149.0	. 754	•	7 1.7	178.4	30
		182.3	•	10501	1.7514	156.4	1.2947		۲2	÷	۰۵
	2	1 46-1	1.6/01	1.60	1.0.0	15,4	1.696	•	1 7510	÷	<u>ت</u>
	70	189•∷	1 • 70 • 1	1 ··· · ·	1.50.54	150.00	1.00.2	•	3	7.	.5
	1.	92.	1.00	497.4	100,000		1.62%		_	C	7
7		•	Ω		1.0.15.	-	?; ;			•	632
٠.,	-	1.1.		4.17	1 . 24 7	164.1	1.5567	•	5	7	1.6402
•	_	ci Ci	1.00.	7.7	· · · · · ·	1	1.4.7.	€	F 7 7 7 7 1		S

		LIRFHAME	LINFRAME PRODUCTION	ENGINE	PROJUCTION	AVIGNICS	AVIGNICS PRODUCTION	ASSMEGATE EXCLUSING	AIR VEHICLE Avionics	10CLUD146	AIR VEHICLE AVIONICS
		TREEK	FACTOR	INDEX	FACTOR	INDEX	FACTOR	* 305 F	FACTOR	X 3CN1	FACTOR
. F R	۲	100	1.900.1	1.010	1. 1446	1001	1.0000	1 0	1.0003	139.1	1.0003
;	;		* * * * * * * * * * * * * * * * * * * *	1 1 2	******	1 1 1	,				
~	31	267.1	1.5661	214.5	1.5207	178.9	1.4540	2.88.2	1.5555	205.1	1.5403
r.	, <u>, , , , , , , , , , , , , , , , , , </u>	210.7	1.5392	215.7	1.0112	180.5	1.4411	211.3	1.5329	208.5	1.5249
~	~	215.7	1.5029	221.7	104703	184.7	1.4480	217.1	1.4955	215.4	1.4879
	47	223.3	1.4523	225.1	1.44.77	168.0	1,57.46	273.1	1.4513	220.2	1.4451
~	79	228.4	1.4219	223.9	1.4117	192.4	1.3517	228.4	1.4203	224.3	1.4150
2	19	:32.4	1.3952	240.1	1.2576	195.1	1.3330	234.1	1, 3066	234.2	1.3821
~	13	238.4	3 0 36 2 2	251.4	1.2465	201.6	1.2906	241.5	1,3455	237.3	1.3408
*	19	256.7	1,2951	288.5	1.1618	2116.2	1.2492	257.4	1,2613	252.4	1.2003
_	ī	258.2	1.2556	302.4	1.1778	217.5	1.1958	268.1	1.2110	263.8	1.2097
r,	. 3	267.2	1.2135	234.3	1.1173	223,8	1.1625	273.2	1,1981	268.3	1.1859
m	.÷.	274.00	1.1808	299.0	1.1898	230.3	1.1294	244.0	1,1592	275.1	1,1567
4	3.5	264.7	1.1389	301.2	1.0820	234.9	1.1673	288.4	1.1257	285.4	1.1242
-	# T	293.1	1.1064	306.8	1.0622	540.5	1.0797	296.1	1.0962	290.6	1.0948
ŗ	~	367.1	1.4805	312,3	1.4436	244.4	1.11642	3-12-8	1.0721	297.0	1.0714
~	11	507.	1.4555	317.9	1.0252	249.A	11.0411	510.0	1.0471	304.0	1.3466
	33	518.1	1.0154	322.6	1.4101	252.7	1.0234	319.1	1.0175	312.4	1.4163
~	€:	323.£	1.5424	324.9	1.0032	259.2	1.0037	923.9	1.6023	317.4	1.0424
~;	17	325.4	0.5975	320.5	U.9483	261.5	1.466.0	325.4	1166.0	313.0	0.9975
•1	ć.	530.3	1.96.1	329.6	0.3387	267.1	0.9759	\$54.1	0.933	323.8	0.9825

AIRF	AIRFYAML FRANUCTINA	E 3t In	PET PRUBUCTION	AVIONICS	AVIONICS FRABUCIION	ASCREGATE Exclud 196	AIR VEHICLE Aviorics	AGGREGATE Including	AIR VEHICLE Avijaics
INDEA	ROE L	1.0Ex	FACTOR	I Ribe A	FACTUR	1 Joe x	FACTOR	INDEX	FACTOR
1900	1.0000	2007	1.0000	100	1.000	1000	1.6363	1904	1.0000
) 		; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;				
161.7	3.186.7	€ C1 0 m	3.1794	162.4	2.5501	111.9	5.1851	101.4	3.1215
167.1	5.4263	167.1	5.4421	106.2	2.4493	197.1	3.0303	107.0	2.972h
113.3	7.58.5	117.3	5.7789	116.6	2,3522	114.4	2.8367	114.0	2.7897
119.0	2.7141	124.5	2,1174	116.4	2,2356	124.6	2.6919	120.2	2.6470
124.4	2.6472	133.0	2.5461	114.9	2.1854	125.6	2.5439	124.9	2.2465
133-2	2.4341	131.1	2.4056	122•н	2.1177	132.7	2.4454	131.9	2.4146
144-1	2.2498	142.3	2.2910	129.4	2.4159	143.7	2.2543	142.2	2.2364
164• n	1.97/5	172.1	1.6931	141.4	1.6396	165.8	1.9573	163.4	1.9470
178.c.	1.8153	142.5	1.7860	149.8	1.7462	179.5	1.8987	176.4 184.1	1.8034 3.728c
194.1	1.0001	243.1	1.0345	161.3	1.6128	9.501	1.6512	195.1	1.5463
208.9	1.5519	216.3	1.5366	119.5	1.4494	210.6	1.5415	207.5	1.5336
23005	1.4060	236.6	1.3774	194.5	1.3377	231.9	1.4000	228+1	1.3947
262.7	1.2343	294.1	1.1082	220.11	1.182e	269.7	1.2057	264.1	1.202.
296.4	1.9934	369.5	1.528	242.5	1.4726	2.44.3	1.6845	293.6	1.0835
324.2	1 - 1 - 1 - 1 - 1 - 1	8.5.8	1.0160	1.00.	1.0001	3.4 · ú	1.0.01	318.2	1.0000

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APPENDIX G ANNUAL DATA FOR THE HISTORICAL INFLATION PROGRAM RAW MATERIAL PORTION ONLY

CALFUDAK VEAR DATA.

*** KAS MATERIAL GALY ***

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APPENDIX H ... MONTHLY DATA FOR THE HISTORICAL INFLATION PROGRAM RAW MATERIAL PORTION ONLY

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e DE	4.43	17.2	1.2.2	•		92.9	0	04.2	ď	4.5	0.1	5.4	9.2	9.1	٥.	Ç.	•	9 0	•
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17001	171.20	1:57.4	1.2 . 7 11		24.1.1	21.4	15.4	.J.E.	٠ ۲	20.	3.6.0	, ,	169.1		•	•	o .	~ ′	
77.46.7	17.1.29	237.4	30.00		240.4	2000	75.4		7.6	ξ;			7 - 90 - 1	` .	= 0	٦, °		` `	
/ /DEC	17.3.00	257.4	10.30		245.9	35. /		<u>:</u> :		֓֞֜֞֜֜֓֓֓֓֓֓֓֓֓֓֜֜֜֓֓֓֓֓֓֓֓֡֓֓֡֓֡֓֓֓֡֓֡֓֡֓֡	- 7 · ·	, c	1001	C •	•	7 .	,	- ~	
2475.	17. 77	25.7.5	14.00				7.4			ָ ֓֞֝֞֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֡֓֓֡֓֡֓֓֓֡֓֡֓֡֓֡	֓֞֜֜֜֜֜֜֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֓֡֓֡֓֓֓֡֓֡֓֡֓֡֓֡֡֡֡	9 0			•	• =	•	. ~	
7 W W T	171.40	250.5	92.90		757.7	55.7	75.4	, E		29	7		170.1	9.6	-	7		~	
13AFR	172.80	254.1	70.51		257.7	15.7	75.4	28•	5 . 1	30.	F . 30	5.3	170.1	5.3	0.	6	•	~	
79KAY	175.46	254.5	92.13		265.	9.87	f-0.9	3.5	3.1	34.	9.10	5.5	172.2	6 • O	•	•	0	_	
1.001.2	174.50	754.7	96.78		263.9	<u>.</u>	8.0 s	٠٥٧	3.1	٠ د: ا	: ·	5	174.2	T.	•		_	~ .	
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7 ENCV	17:40		66.93		275.0	=	*;	,	7	36.	6	32.5	٠,	0.0		Ξ.	_	_	
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1.144.1	19.00	275.7	18.5		5.1.5				Ξ.	3.	6.5.	01.1.	19.8	5.1	=	7		7	
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LA638-	rifer	56.7X		.00	00.0	2000	00.1	J. AA	J.00	10 ° 0	. D.C.	00.0	0 · 0	0.00	1.00	0.000	0	•	•	30.0	0	0	~	3 °	3 (- 0	20.0	30.5	00.	0.00	J. 10
	116. KX	. L. t		153.40	0: 0:1	157.04	158.10	100.10	11.7.69	163.00	101.73	162.00	163.70	164.23	166.50	165.70	165.80	167.40	170.20	170.50	170.40	170.69	170.70	171.40	00.4/1			94.01	0/10/1	173.64	175.90	175.90	176.40
	25.45.KK	1.411.		14.63	64.63	35.37	39.83	91.10	93.00	64.53	65.4F	56.4€	22.30	322.90	355.93	63.50	03.50	366.69	14.83	14.80	14.90	117.90	377.99	377.90	581.60	561.00	00.000	00.27	00.07	15.50	170.20	170.20	70.26
	20 May 2	1010) } ! !	19.70 2	79.73 2	79.73 2	73.74 2	19.76 2	13.71 3	15.7.1 2	11.54 2	364.40 2	77.50		=		9	ے			377.50 3			. B.13	_	•	= ·	۵. د د د		77.54 3	17.50 3	77.50 3	77-50 3
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		*NTX EX	; ; ;	62 34.6	6.7 (14.4)	62 93	02	200	20.7	44.00	3.64 59	9.Eu 50		4.56 30	1.54 30		4.56 30				4.50 30									4.26 30	4.56 3d	4.50 311	4.50 37
		3		70 26		2.5	7 : 76	7.5	7.0	71. 7 11.5	21 20	211 211	. R. J. 1. 1. 1.	10 22	60 22	.6il 22	30 22	.54 22	.9(22)	.90 22	.90 22	10 22	31, 2	.73 22	11: 22	έ: -1:	10 22	1. 22.	411 221	40 25	41, 22	.41 22	411 224
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HA1E	121162	MALLIE 3	1 1 1 1 1	322.70	122.74	199.7	100.74			347.70	347.76	141.73	147.70	347.79	547.7	347.70	347.74	372,78	312.70	572.70	372.74	312.71	372.71	372.70	312.74	312.76	172.70	372.74	372.70	374.70	372.10	372,76	\$12.70
	22.11.2.1	Like		3 < 1 . 4 0	20 TO 10 TO	303.16		2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	100	17.5	314.56	88.16V	16.54	214.19	257.10	271.40	264.34	271.40	256.40	321.40	307.10	272.50	253.00	521.48	221.43	214.53		1590	187.30	165.76	192.10	165.30	156.44
	_			344676	34 70		1 1 1 1 1 1	7	456.4		357.91														101.10	491.16	401.10	400.50	480.50	400.59	399.64	399,61	359.60
1	15 (141 15135)	CAST		115.511				30.4.4					5 to the tr	14 5, a 8 11	347.20		345.311	36.B. Bu	366.18	370.6.1	3/1.640	303.60	3/5.86	345.48	366.70	346.31	16.6.68	403.504	413.4	415.41	415.60	415.61	410.63
	5 1362£4	SINLS CAST	1	40.00 C																					237.53					247.50			
	2 411071	10 %													523.40		323.19								1140000				143.60				
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A TENT TO THE TOTAL TO SELECT

APPENDIX I HISTORICAL INFLATION INDICES RAW MATERIAL PORTION ONLY

HISTORICAL TUFLATION FREETRON FREETRON

The proposition The propos		•					STATES AND STATES
1 HBF X FACT 2R TYDEX FACT 2R TYDEX		AIRFFAHE	PRODUCTION	£ 56 10f	PROUDETT 34	FXCE X IN	5 AV10:41CS
CY67= CY67= <th< th=""><th></th><th>INDEX</th><th>FACTOR</th><th>x 202.1</th><th>f Ar Trie</th><th>x 3ún I</th><th>FACTOR</th></th<>		INDEX	FACTOR	x 202.1	f Ar Trie	x 3ún I	FACTOR
CY 1PU.** 1.600 ft. 100.00 1.600 ft. 47 17.01 4.5240 36.2 4.8479 21.5 49 19.5 3.9837 4.2270 24.2 41 26.4 4.554 4.564 4.245 24.2 51 26.4 4.57 4.0141 24.2 24.2 51 27.3 4.67 4.0141 27.4 27.4 52 27.4 4.0141 27.4 24.4 53 27.3 48.7 3.6014 24.4 54 27.5 2.2614 3.4623 24.6 54 23.6 3.07 3.4623 2.463 2.466 54 27.4 2.607 2.995 2.995 2.995 2.995 2.995 54 27.4 2.746 2.995 2.995 2.995 2.995 2.995 54 27.4 2.795 2.995 2.995 2.995 2.995 2.995 57 </th <th></th> <th>CYE7=</th> <th>FYK2</th> <th>CY 5.72</th> <th>E 7 : 2 = 2</th> <th>CY37=</th> <th>FYB.</th>		CYE7=	FYK2	CY 5.72	E 7 : 2 = 2	CY37=	FYB.
47 17-0 4-5259 36-2 4-8479 21-3 48 19-3 3-9834 41-5 4-2470 24-1 41 19-3 3-9834 41-5 4-2470 24-1 41 19-3 3-9834 41-5 4-2470 24-1 41 20-45 4-2470 2-4-1 24-1 41 20-45 4-2470 2-4-1 2-4-1 41 20-45 4-2470 2-4-1 2-4-1 41 20-45 4-240 2-4-1 2-4-1 42 20-44 3-644 3-644 2-4-4 2-4-4 43 20-44 3-644 <t< td=""><td><u>ب</u> ن</td><td> 0 . 1</td><td>1.000</td><td>100.0</td><td>1.4400</td><td>1. C. J. J.</td><td>1.6001</td></t<>	<u>ب</u> ن	0 . 1	1.000	100.0	1.4400	1. C. J. J.	1.6001
44 17.0 4.5267 56.2 4.8479 21.3 44 19.2 4.0037 41.2 4.2401 24.1 41 19.3 3.9837 4.0141 24.2 51 20.4 3.7456 48.7 3.6145 29.7 51 23.4 3.3451 48.7 3.6145 24.4 53 22.3 3.2811 48.7 3.6145 24.4 54 23.5 3.2853 56.8 5.4895 24.4 54 23.6 3.0348 56.8 2.9850 2.9850 2.9850 54 27.4 2.785 56.8 2.9850 2.9850 2.9850 2.9850 54 27.8 2.785 2.785 2.9850 2.9850 2.9850 2.9850 54 27.8 27.8 2.785 2.9850	;	1 1 5	1 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	;	1 1 1	•	
44 19.2 4.00 (3) 41.5 4.2401 24.2 51 20.6 3.7456 41.5 4.0141 27.7 51 20.6 3.7456 43.7 4.0141 27.7 51 27.8 3.2457 4.017 3.6485 24.8 53 22.3 3.2453 56.3 5.4896 24.4 54 23.6 3.0346 54.0 3.4623 24.4 55 25.6 3.0346 54.0 3.2452 2.4.4 55 25.6 3.0346 54.0 3.2452 2.4.4 56 2.5676 54.1 3.2452 2.4.4 2.4.4 56 2.5676 54.1 3.2452 2.4.4 2.4.4 57 2.7.4 2.7.4 2.7.4 2.7.4 2.4.4 2.4.4 57 2.7.4 2.7.4 2.9.452 2.9.452 2.4.4 2.4.4 57 2.7.5 2.7.5 2.7.5 2.7.5 2.7.5 2.7.5 2.7.5	;	17.0	4.5259	36.2	62 48 . 4	21.3	4.6483
44 19.5 3.983V 41.5 4.2273 74.5 51 20.6 5.7456 43.7 4.0141 25.7 51 27.1 3.5045 3.6046 27.4 52 3.25617 44.7 3.6014 24.4 53 27.8 5.2647 5.4696 24.4 54 23.6 5.2559 50.7 5.4623 24.4 55 25.6 3.0346 54.1 3.2402 21.6 54 27.4 2.80092 2.7545 2.9450 2.9450 54 27.5 2.7545 60.0 2.9262 2.9450		19.2	4.000.4	41.2	4.259	24.1	4.1.144
3.1 26.6 3.7456 43.7 4.0141 20.7 3.1 5.3349 48.7 3.60485 24.6 5.2 3.2617 48.7 3.6014 24.6 5.3 27.8 5.2559 5.4696 24.6 5.4 23.6 5.2559 5.4623 24.7 5.5 25.6 5.407 3.9452 24.7 5.6 2.867 2.9850 2.9850 24.7 5.7 27.4 2.7545 2.9850 2.9850 24.7 5.7 27.8 2.7545 2.9850 2.9850 2.9850 2.9850	•	19.3	3.984	41.5	4.2270	0.00	4.0301
11 23.41 48.7 3.6445 20.45 20.44 52 3.26.11 48.7 3.6414 24.54 53 27.85 3.2835 5.4695 24.49 54 23.6 3.0348 5.4623 24.7 55 25.4 3.0348 54.2 2.9850 21.6 54 27.4 2.6002 2.9850 24.3 24.3 57 27.9 2.7549 66.0 2.9252 25.9262 25.9262	ī,	20.0	3.7456	43.7	4.0141	20.1	3.8471
52 3.26.13 4H-7 3.60.14 24.56 24.56 54 23.6 3.283 5F.55 4.4696 24.69 24.69 54 23.6 3.2559 30.77 3.4623 24.7 55 25.9 3.0346 54.1 3.2427 21.8 54 27.9 2.7545 66.0 2.0252 44.4 57 27.9 2.7545 66.0 2.0252 35.0	÷	23.1	5.3349	48.7	3.6845	ਲ•ਲ∂ *	3.4362
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23.6 5.2559 50.7 5.4623 2.4.7 25.4 3.0342 54.1 3.242 71.6 27.4 2.6072 56.6 2.9850 74.4 27.9 2.7545 66.0 2.4262 85.0		2.5	3.2835	5 · 3 · 5	76840	# * T \	3.3617
25.4 3.0348 54.1 3.242? (1.P. 21.P. 27.4 27.4 2.8002 556.8 2.9850 (4.3	ν. •	23.6	5.2554	5.00	3.4623	7 * - 3	3.3543
27.4 2.8002 56.8 2.9850 14.4 27.9 2.7585 60.0 2.9562 80.0	Ş÷	25.4	3.8348	54.1	3.2422	d • [v	3.11.55
27.9 2.7545 66.0 2.4262	r. T.	27.4	2.8092	9.86	2.9850	₹ • ₩ ₂	2.4759
	5.7	27.9	2.7585	9 + 0 4	2965	8.5.4	2.8225

MISTOPICAL TUFLATION CALFUDAR YFAR THOLFS

						AUGHEGATE	ALA VENICL!	ASCHEGATE	AIR VEHICLE
AIRFRAME	AIRFRAME PRODUCTION	ENGINE	PRODUCT104	AVIONICS	FRODUCTION	EXCLUCING	AVIOUICS	INCLUDIES	AVIONICA
1 10.05	6.0176.3	X.1351	F A C I D R	1205 x	FACTOR	X 3 C # 1	FACTOR	N 3CN I	FACTOP
, K 2 - L		= Z 9 X J	1 4 14 3 E	C.Y.6.7:	FY 8.2 =	51913	FYHZ=	C Y < 7 =	FYRZ=
1.66.1	1.6000	1000	1.0000	100	1.0000	1,19,1	1.64.01	1.4.1.	1.011
 								1 1 1	
1.76	2,1762	7.63	2.9456	31.5	1.7497	x • 4 %	2. H40f.	34.1	2.7401
25.0	20,42,0	1 4 4 5 1 4 6 5	3,1177	3143	1.7528	32.5	3.0542	32.5	2.910,
26.2	1616	51.9	3.1292	8.0.8	1.77.0	33.2	2.9741	33.4	2.8619
	3.0315	57.0	3.4791	30.0	1.7764	32.4	3.0501	\$2.5	2.9279
	30.130.5	50.00	3-1435	34.5	1.8935	31.5	5.13.2	31.4	3.4.776
23.7	1,25,49	53.2	3.2964	30.1	1.8224	33.2	3.2711	30 • 2	5.1265
. L. C.	1,2698	3 6 5	3.5252	39.0	1.8339	4.66	3.3660	29.4	3.216
23.6	3.26.24	0.64	3.5788	311.0	1.8339	29.3	3.3803	29.3	3.2223
23.1	4.2 404	8.04	3.5255	8 ° C F	1.7851	23.6	3.3419	29.7	3.1793
24.4	3.1934	52.P	5,3227	31.5	1.744)	31.	3.2432	31.6	3.1588
4 4	5.141.5	 1 45 1 16	3.2295	31.2	1.7591	31.1	3.1759	31.1	3.1336
2.50	5-0184	57.6	3.6353	31.7	1.7319	32.7	3.0259	32.5	2.8992
26.2	2.934	4.55	2-6874	31.8	1.7267	34.9	2.8318	34.5	2.7502
2.96	2.9433	67.7	2.5729	32,3	1.7031	35.4	7.927	35.1	2.6925
26.5	2.89.5	9°04	2.65.3	32.6	1.6867	33.5	7.794!	35.1	2.5959
27.53	2.8226	666.7	2.6514	32.9	1.6795	35.9	2.7525	35.6	2.6526
24.2	2,2539	H2.9	2.1175	35.1	1.5655	4.7.0	2.1381	6.44	2.1476
1.51	1.9678	96.7	300	46.4	1.5100	51.7	1.9123	50.2	1.8831
60.0	1 P P 2 2 5	1 16.8	1.7407	36.5	1.50%	5.034	1.7595	53.	1.7700
1 · · · · · · · · · · · · · · · · · · ·	1.6833	1111.5	1.5733	37.h	1.4594	61.7	1.6913	58.	1.6295
2.04	1.5637	113.2	1.5495	4).4	1.3743	63.5	1.5581	61.1	1.5469
7 6 6	1.38.5	130.2	1.3479	42.4	1.2842	72.7	1.5704	69.2	1.3651
7 9 9	1.1907	170.9	1.0265	4.3.2	1.1158	46.3	1.1209	84.4	1.1198
, • • ·	1.0277	173.0	1.0144	53.0	1.4375	94.1	1.0224	92.5	1.0233

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MISTOPICAL TURLETT STORY

		AIRFRAME	PROCUCTION	314 I 91-3	PRODUCTION.	AVI: 110	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		SOLNOIN S	1 M C 100 1 20	
			A C I	105	FACIOR	11. TX	140108	I UDE X	FACIOR	* 45. P. I	<u>.</u>
		CY67=	· N	CY67=	TO MA	CY672	1112=	LYP. 7:	FYHZE	CY 1.7 =	FYAZE
ں	-	-	٠,	٠	1.6936	1.10	1.00.0		۳,	· · · ·	€.
•	•	:	;		1 1 1		•	:			
£	-	24.	37.	4.50	•	*1.	1.7.15	; • D •	~	54.4	1.1041
•	٠ -	24.	7.3	12.4	2 6 5 4 7 2	*: -:	[-14]	4.1.5	• 25E	50.5	<u>-1</u>
SEP 6	·-	2	.19	72.4	•	\$1.5	1.752F	4 ° C '	.251	* • U	166.
4	, ,	ů.	-18	53.7	•	.1.	1.754.	11	۲,	£.08	16.7
L	٠	N	-1	54.1	•	۲۰۱۶	1.7598	5.3	.19	33.3	4.5
w	٠	24.	.16	1.40	3.2423	3.13	1.7451	3.1.9	3.1003	31.0	0
4.	عد	24.				31.4		31.1	-	31.1	038
æ	دي دي	24.	.13	5.0	3.2226	31.1	1.7545	31.2	.16	31.2	ŝ
ų.	ų. E	24.	.13	54.5		71.	1.753H	31.2	7	31.2	137
Ġ,	·O er	24.	.13	*	3.2260	31.5	1.7545	31.2	3.1713	31.2	_
٠٢.	æ	2.	.16				1.7528	51.9	-:	31.1	145
٤	1 0	24.	÷	54.4			1.7598	31.1	7	31.2	~
£	.n	24.	.12	*			1.7516		-	31.3	_
ũ	æ	2.	.:	54.6			1.7616	31.1	7	31.5	~
ī		7	-	54.4		31.5	1.76.16	1.1.	3.1793		5.937?
S.	4	24.	-	54.4	. 22	31.3	1.7610	31.1	3.1785	31.1	=
£	•	24.	•	54.1	3.2422	31.7	1.7598	1.1.	3.1820	31.1	1.0392
÷	æ	24	•	54.1	~	51.5	ニケビレ・ロ		96/1-1	31.1	=
ų	ar ar	24.	.12	15.1	7	31.2	1 - 76.54	51.5	3.1545	31.5	HE6.
Ü	÷	25.	• 16	55.7	-	31.4	1.7405	٠٠,	3. 125.1	31.9	. 96
\$	e	25.	• 0.	3.50	∹	31.0	1.7371	ر. . • د	3.0873	32.3	•
9	S	25		96.0	3.1341	31.7	1.7356	ر. • در • در	- U 7 -	35.2	٠
÷		25.	5	56.1	-	11.1	1.7434	.	• C ÷ O	\$2.2	•
¥	T.	25	1:-	5,1.2	٦.	31.7	1.7316	 	3.0351	32.5	•
ū	~	25.	Ę	51.5	4.0.FH	51.7	1.755	35.6	ć	€-25	2.9:43
¥	۲	25.	.98	5.16	150	31.7	1.735.	3.7.7	5	9.02	٠
4	-	25.	. u	6.49	5.0831	31.9	1.72:4	۲۰۰ ٤	•	35.5	6116
Ü	~	25.	• 68	11.2	2.8581	31.7	1.71.44	35.5	4.0	33.4	.828
Ü	۲ (25.	8.	51.0	٦.	37.4	1.7144	35.6	• 94	33.5	. H 2 4
Ġ	,	24.	6	4.1.6	2.7522	31.9	1.7193	10.5	2.P59H	34.2	۲.
-	~	26.	40.	1.54	2.6344	31.7	1.7199	34.8	٠٤	•	
ř.	~	2¢.	40.	1.50	÷	31.4	1.7475	34.8	÷	34.5	-
~	٠ ا	26.		100	1.4.3.2	31.6	1.141.	34.	5.43.	3	۲.
_	7	96.	. 43	1.5.1	÷	11.1	1.7556	3 • 4 60	H 2 4 .	3	`.
~		26.	7.9744	1.00	•	51.4	1.7475	· · · · · · · · · · · · · · · · · · ·	7.7	*	~
-	-	36.	2۲.	2.00	•	51.3	1. 7. 2.2	1. • ··	נ כ ש	14.7	•
~	_	56.	. 43	· · · · ·	. 6.3	٠.١٠	1.61.1	. • . ,	۲.	34.	٦.
~	~	۶,٠	٥٥.	C. • 4 ::		*11.			•		~
-	_	26.	رن ا	**		3,0,1	1.71	7 * 7 %	÷	. 64	~
-	,	2.5	.93		71 T 11 '5 * C	5.5	1.11.2	- 47	2.8.5.1	34.5	
~	`	36.	0					•	٠		,
		•					: ·	•	•	- " 7 "	7.11.

HISTORICAL TOFLATION FOUNTHLY INDICES

		AIRFRAME	E PRODUCTION	ENGINE FR			VIUNIUS INDOCUTION		AVIUNICO		4 V 1 V 1 L C S
		INDEX	FACTOR	¹40€	AC F	INDEX	A C I	1 no Ex	FACTOR	I NUE X	ပ
		J	۲ ۲ ۲	CY67=	>	C Y 6 /=	Y #2=	CY 57=	P 2 =	C Y 57=	FYBOR
	CY FY		Ē	0		109.1	.000	•	0.0	Ξ.	
		•		; ;	!	1 4		: .			1 6
				F 6	• th.	5 J	٠,	T 0	20.04.0	7.44	7.79
			. 0			0.00	נימל		2.60.7		71.
				0	200	30.5	691	\$ 0.5 \$ 0.5	2.1974		2.6343
			91.	٠.	6.77	4.00	.69P	(F)	2.7939	35.1	9
			916	•	5.5	32.4	1.6932	35.8	2.7635	35.4	•
			.914	æ	.554	32.5	691	35.8	2.7511	35.3	. 663
			.914	τ	554	32.5	• 6A9	55.₽	2.76.33	35.5	• 65.2
SEF			.917	9.20	• 556	32.4	969	S. S. S.	2.7558	35.4	•
			•91к	æ	• 55	32.4	•	₹5.8	2.7641	35.4	. 556
			.922	$\boldsymbol{\tau}$	• 55	32.3	•	\$5.7	2.7562	45.4	•
			.924	œ	Ç.	32.3	. 791	55.7	2.1122	55.5	•
		26.	•934	T)	• 56	32.3	1.793	35.6	2.1765	35.0	٠,
		•	• 905		•	32.6	•	6.05	2.7.68	35.5	÷,
		•	. 96.	9.69	•	32.6	• 6 A 6		2.7481	35•6	•
		•••	• B 9 4	69.0	•	32.5	1.693	٠.	2.7471	35.7	٠,
		••	.886	9.69	2.5422	32.8	٠٠.	55.	2.7599	35° H	•
		•••	• A P E	٠	•	32.1		85°E	2.8221	F	•
		•	.891	*	•	32.8	1.6763	3°1• 0	2-8235	2	` '
		•	• #B	~	•	32.7	1.6815	٠	2.8357	34.5	•
		•	. AE5	63.6	4.7.F	32.5	1.5883	•	2. H338	24.1	•
		•	.694	3.6	. 7.h	32.5	1.6839 	•	2.8592	5 .	•
			.892	63.65	. 75	32.5		x :	2.63.42	34.5	• '
		. • .	. 892	63.6	. 75B	32.5	3	•	F104.7	£	•
			T. T.	5.7	67.5	N I	.	T • T •	1468.3		`.'
			. 35 FB 7.	1.54	6.7.	~ ∘		•	2.48331		
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		٠.	000	0 · C	1659.2	v	1.6765	F (1)	2.7494	100 100 100 100 100 100 100 100 100 100	י פרים פרים
				6.7.0		0 0	•	36.0	2.74.53	15.7	
		•	. B. 3.	J • 1 · 5	`		٠	36.00	2.7444	35.1	• 64
			. A 2 E	07.0		32.9	.667	* i, . 1	2 • 7 4 .15	35.8	Ý.
		•	. A D 1	61.5	6.61	0 0.27	1.661	5 3	2-1233	36.1	, 6 ,
		•	. 7 H 4	61.	2.6106	35.1	1.65.41	4.00	2 - 7 1 51	36.1	•
		•••	. 75	(1.)	2000	33.0	1.66.25	16.7	2.6938	36.3	
		••	٦.	67.6	2.5960	13.4	•	1.7.1	2.6563	36.7	.574
	•	74	.627		4. 5.5.7		1.649.7	٠٠٠	36t 3°C	~	.5.14
			-6-	- • · · · · · · · · · · · · · · · · · ·	* T # 5 * 5	*: • :: \$	-	-	2.5794	37.4	*
		-	ς.	5. 1 .5	2. 1.5		1.6.262		9.4354	- 6 6	2.4211
		~,	• 42	1.4.	٠.	1.0.7	=	٠,٠,٠	~ + T + · · ·	46.	• 5.4
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		•	`.	1.		7	1. 0.0 1.	; ;	<.	, , ,,	2.1735
706		•	7-16-7	•	÷.	٠ <u>٠</u>	1.5	4	2.1.11	•	2.1155

HISTORICAL INFLATION MONTHLY INDICES

			2	FACTOR	3OF	FACTOR	INDEX	A C I	x301.1	FACTOR	X 30% I	FACTOR
		J	S	~	CY57=	FYAZ=	CY07=	F Y 92=	CY57=	F Y 8.2=	CY67:	F Y 8.2=
	נא	>	163.	٠,	100.0	10 to to 1	100.0	000	100	1.6000	107.0	Ë
:	•		i	1	!!!!	,			1	1		1 1 1 1
904	_	75	;	2.0876	91.2	1.9240	35.9	1.5312	0.64	2.0199	41.5	383
٩	_	75	ġ	• P84	91.5	1.9179	35.7	1.5195	49.0	.015	47.7	C
5	_	75	;	• 13 £	4.5€	1.4941	36.5	1.5258	50.0	1.9795	48.6	\$ 5
> 0	_	75	-	.046	32.A	1.8903	36.8	1.4932	4.4	1.9414	9 • G &	1.3443
<u>د</u>	_	75		. 653	43.6	1.4743	36.9	1.4906	J•195	1.9786	4.9.7	1.9417
4	_	25	8	865.	98.8	1.7157	36.9	1.4868	51.3	904	59.4	1.8738
3	_	75	æ	.00.	35.4	1.3208	36.9	1.4906	51.4	1.9255	5.00	1.8332
, «		75	ď	666	36.2	1.8241	16.7		51.3	1.9266	49.3	1.8943
~		. <u>.</u>	4	166	96.4	1.8202	35.6	1.4936	. · 1. ·	1.9195	5.4.4	1.9387
` \	_	2.5		. 67.	36.0	1.8192	- A		51.9	1.9056	51.3	1.8769
· <u>*</u>		· 5	5	973	95.2	1.8456	36.4		51.5	1.9203	51.	1.8902
-	_	2	6	176		1.84.07	36.4		51.6	1.9177	59.0	1.3879
1 12		<u> </u>		610	4.0	1.8391	36.3		52.1	1.9984	54.5	1.9709
	`~	ي ر	6	936	9.00	1.6839.1	36.1		32.1	1.8971	59.	1.9704
-	_	9/			97.6	1.8419	35.3		52.0	1.9121	50.4	1.8757
· >	_	9		942	9.5.6	1.8700	36.0		51.7	1.9132	50.1	1.385.5
		9.	6	-	8000	1.6711	36.0	•	.1.5	1,9145	50.1	1.8865
-	_	76		.913	38.7	1.7786	36.1	1,5241	53.1	1.861.	51.4	1.6373
60	~	9	ë	.912	98.1	1.7705	36.2	•	7.9 ° ₹ ½ ₹ ½	1.8573	51.5	1.8332
0 7 F	_	76	40.6	1.8959	66	1.7687	36.2	1.5165	53.6	1.8442	51.9	1.8213
Œ		16	;	.887	33.2	1.7682	36.3	1.5137	5.5 • 8	1.8383	52.1	1.8157
_	_	9,	-	.853	3.66	1.7665	36.0	1.5124	₹ • ₹ ;;	1.6183	52.6	1.1972
Ξ		9		.82h	4.50	1.7547	16.5	1.5460	6.40	1.9118	53.3	. 793
=			ż	•	9 4 6	1.7546	3a.5	1.5434	55.1	1.7959	5.8°2	1.7759
9	_	1.	ζ.	_	102.5	1.7113	36.	1.5047	56.5	1.92.1	G • \$ 5	1.7429
.				•	=	•	36.4	1.5003	6.1.2	1.7241	5.00 6.00 6.00	1.7130
5			÷	•	103.2	1.7005	36.8	1.4732	51.3	1.7267	55.2	1.7111
>	_	1.1		•	1.13.2	1.6499	35.8	1.4019	7.11.	1-7232	5.54	1.7124
ب	_	~	;	•		1.17.11	36.0	1.486-	1.7.	1.7118	55.1	1.7145
ž	_	11	*	1.75.9	4.721	1.6632	37.2	1.4755	1,7.5	1.7164	55	1.7402
89		1.1	;	•		1.4327	37.3	1.4750	H • 1 ',	1.795	55.8	1.6937
¥		11	;	•		1.61.182	37.3	1.4742	ند ند ا	1.6828	56.6	1.6490
œ	^			•		1.6176	31.5	1.466.	** 7. 4	1.59.1	5.7.4	1.6475
<u>_</u>	_	~		1.0941		1.55H3	37.4	1.46.8	• • • • • • • • • • • • • • • • • • • •	1.4 578	1.4.	1.5269
N('C	_		45.5	1.69.46	5 · S I I	404.	2.4	1.42.54	•	10. 123	5 6	1.6217
ب	^	11	÷	1.66.75		388 - H	57.4	1.4673	*• [:]	1 • 6 0 9 3	- σ σ	1.4343
9	~			1.656.	114.6	1.542	57.4	1.46.27		-	200	1.576,
u.	~	11	46.	1.655.	115.5	1.045.	F. • 71	1.447	. I u	1-11:1	- z.c	1.654.3
_	_	:	٠c	6. a	113.6	1.4940	- · · · ·	1. 44.1	. 1 •	1.614)	7 • 74 E	1.54.32
>	^	7	46.1	1.5512	115.		·.	1.4.1	5 · 1 ·	1.6:11	1.0	1.5197
د	_	1		Ĺ			. • , ,	1.44.1	* 1	1.113	· · · · ·	1.5946
<u> </u>	^	4	,	. 4		174				[•	1.5.717
											•	

HISTORICAL TEFLATION NOWTHLY INDICES

		AIRFHAPE	AIRFHAME PRODUCTION	EUS INE	PRODUCTION	AVIONICS	AVIONICS FRODUCTION	AGSREGATE EXCLUPITES	ATP VEHICLE AVIONICS	AGGET GATE INCLUDING	AIP VEHICLE Aviduics
		1 NOF X	-	14.06 %	FACTOR	1 MDE X	FACTOP	INDEX	FACTOR	30	ACT
		CY67=	F Y 82=	C167=	FYB2s	CY67=	FYY?=	CY67=	FYRZ:	C Y 6 7 =	イカンド
J	۱.	۲ ،	-		000	160.)	1. 14 18	:	31.0	-	000
	•		;	!	1 1 5	!	1 1 1		;		H
¥	_	æ	_	:	•	r.	305	54.5	S	ار ا	<u>`</u> ;
<u>ب</u>	^	÷	.587	10.	•	÷	391	62.3	.536	69.1	, ,
	~	9	.561	=	•	6	1.3841	1.5.3	S.	60.4	5
	_	æ	.573	112.9	1.5539	39.9	1.3734	63.2	1.5657	8 · 0 ·	ic.
	Γ.	α,	1.55211	114.4	•	ċ	1.1721	5.4.8	S	61.4	2
	~	Œ	C.	113.3	1.5222	=	1.3732	64.6	s	62.1	1.52.4
36.0	~	Z)	ς,	$\overline{}$	•	_	1.3711	•	1.5312	52.1	3.
	~	ŗ.	Ç,	-	•	C.	1.3572	3	1.5.529	52.1	1.5214
	~	.	Ĺ	-	•	~	1.3415	1.4.5	•	62.3	2
	^	9	1.5133	115.7	1.517"	£	- ,	8 . 6 9	1.5148	62.3	1.5035
	~	6	·C	-	٠	-	337	8 • C a	1.5018	6.5.4	7
FEU	_	6	4.9	-	1.4796	41.3	329	€445	1.4865	64.1	3
	~	_	•	_	•	-	•	67.2	1.4709	64.7	40
	_	6	1.4123	;	٠	~	1.3142	6.69	1.4140	67.1	Ξ,
	_	8		126.5	• 365	~		11.4	1.3842	x	~;
	7	÷	1.3855	131.2	1.3374	\sim	56₹	72.3	1.3485	6	Α,
	-	6	•	133.9	•	•	1.2777	73.5	•	•	÷.
AUS 7	_	5	1.3626	1 34 . 7	1.3027	43.2	1.2721	73.3	. 338	ċ	5
	~	•	-,	134.8	٠.	•	1.2511	73.9	338	5.0.	5
	J.	c	7	1.201	_	4	1.2456	7 2	1.2651	7.47	52
>	37	•	?	161.2	2	4	1.2385	 	1.1385	78.7	- '
	æ	_		151.4	•	· •	1.227.	ر م د د د د د د د د د د د د د د د د د د د	1.1924	70.1	œ,
12	æ	•	•	161.9	•	46.1	1.1923	1	1.181.		181.1
7,	Œ:	ے	r.	C . Z	•	47.2	1.16 %	9.1	1.0949	5 · 5 cc	= '
	T.	ے	1.5278	- 6 - 7	0.0522	47.5	1.1514	ъ.	1.7315	×6.	1.094
	u.	= -	1.1931	168.9	•	# · ·		1 - 1 - 1	1.177	Tier of	1.1275
4 7 .	x :	٠,	-	T (٠	7 · ·	00011	\$ • • • • • • • • • • • • • • • • • • •	56.7.1	60.0	
	 	.; e		- 0 x 4 x 4 x 4 x 4 x 4 x 4 x 4 x 4 x 4 x	F5.0.1	C 7	2 - I - I		1.1226	r r	10101
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	~	ء .		•	1. 172	30.00	_	: r c	1.11.11	34.7	1.1152
	Œ	_	1.1577	168.3	1.1426	56.35	1.3453	1	1.1.194	85.5	1.1089
	τ	_	1.15!.R	167.1	1.061	=	1.1810	4.)• 3	_	85.4	1.1057
	ູ	1 66	1.1514	153.9	1.0703	<u>. اد</u>	1.77	5 •	Ξ	7.32	1-1156
J41, 8	Œ	1 70	1.61.1	J. p. 1	1.7353	5.13	1.0554	60.	n 7 s	84.1	1.0709
		1 7n	1.60.1		3	6.1.7	1.9621	ن ، ۱ د	. 7.0	83.	1.0715
		_	1.0515	111.2	1 . 1,47	\$ • • ¢	1. 4 1	1-1-1	-	9 ° 0	ς-
		1.	1.074.3		1.0178	•	1	· •	٠,	91.4	J
		_	1.63.1	172.	1.1.1	• • • • • • • • • • • • • • • • • • •	<u>-</u>	٠ ٠ ٠	10,001	91.9	1.6291
		_	1.12	1.11	1.104	7.00	1.14]	`.'	2	30.6	1.9173
_		1 14.	-	1.4.1	1. 1/3	•	7.50	- :	1. n 7.	1.5.	
500	· -	1 700	1 - 1	1,4,1		1.1	1 1	 :	1 • 1		1.0.17
2	7 =	1 16.0	1. 1. 4.	1.44.7	- -	·	1. 21.	· · :	* · · · · · · · · · · · · · · · · · · ·	• • • • • • • • • • • • • • • • • • • •	, T

HE FOR THE CONTRACTOR

THE ALM VEHICLE AGGREGATE ALT VEHICLE

			REFFERNE	RISPRANE FESTIVATION		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		14500 C 1 134	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	STREAM	INCURDING	AVIONICS
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			C Y 6.7=	1: CH M 19	CY L 7		- 1 1 L	1 1 182:	11013	F 16	21 18 3	FYBP=
	٦	-	1001	1.4444	1000	1.000	1 444 . C	1.9952		30.0-1	100.0	1.093
:	•	;			1 1 1			: : : : : : : : : : : : : : : : : : : :	:	1 1 1	:	* * * * * * * * *
	-	:	76.9	113,,*1		1 29	`.;	1.0201		1.00134	3.4.5	1.00 %
\ 01	-	. .	11.0	£ 404.	1.4.4.	15100	4-16	1.23.1	D • 9 t	1.643	34.1	1.00.1
•	74	1	11.1		1 /4.	1.04.7	0.4.0	1.0017	, • • p	1.9912	5.46	7.9984
240	82	 F	17.3	8 O	, • · · . I	1.3056	9.64	50 Cu 0	** ***	13.000	34.)	9.3952
	n.	· .	C * X /	F. Ko * 1	17.	964.50	• 15.4	11 966° j	1.66	0.01.00	95.1	4266.9
3.7	42	a. ~-	11.5	1 1 4 0 ° 0		1.4413	67 * 4.4	1866.0	5.66	ħ . ξ; •0	95.1	0.9934
?	ti. at	·.	11.4	J. 944.		(394.)	5.4.5	C\$ 66 P	2. a. s.	· *15 * 1	9.43	9342
1 4	e B	÷.	16.0	1.69.1	1700	1,0000	, , ,	+ 160°b	***	1.1764	5.96	£ 5, 6 to 0 1
<u></u>	 T	<u>.</u>	76.5	1.6.16.3	111.01	9.4953	\$ 4.7.5	18 3 5 5 E	1	1.0115	7 . 77	1.9104
ڌ	?	4	16.	- 133	: • : · -		4.4.0	ាះ ១៨ 🕶 មែ	^ • • • • • • • • • • • • • • • • • • •	1.1000	41.7	1.400
 4	Ņ	-; 3;	16.0	: 1:1-1	. / .	14 6 6.6. * *	0 • •	. I 50 ° d	·.•	1.9.1	~	1.00.4
	<u>ئ</u> ج		10.4	1 - 31 54	17.	10000	55.	H . 9 41. 7	7.	1.01.0.1	9°	1:0.1

MISTORICAL INFLATION GUARTFRLY INDICES

PACTOR TRDEX FACTOR FACTOR TRUEX FACTOR TRUE		AIRFRAME	IRFRAME PRODUCTION	ENGINE	PRODUCTION	AVICNICS	PRUDUCTION	AG SPECATE EXCLUDING	AIR VEHICLE Aviorics	ASGREGATE TACLUDING	AIR VEHICLE Avionics
		INDEA	ACTO	2	010	I NDE X	FACTOR	LIBEX	ACT	T RDC K	FACTOR
TR CY 100.0 1.00.1 100.0 1.		CY67=	Y82=	¥	E CHA	C 1 & 1=	7 N 2	۲ ۲۶	# X X	= / (.)	1 2 P A
7.7 24.5 3.1995	۲	196.	. 000	<u>.</u>	=======================================	Ē	: ·	-		1 a.i., 1	•
6.7 28.6 1 2.1995 52.6 6.8 1.995 52.6 6.8 1.995 5.9 1.995 5.0 1.995 5.0 1.995 5.0 1.995 5.0 1.995 5.0 1.995 5.0 1.99	;	:	-	;		1 1 1	:	!!!!	:	:::::::::::::::::::::::::::::::::::::::	:
6.7 24.5 3.117.3 54.6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	۲,	24.1	.199	ċ	.347	31.4	4	4	5.5	3 n .5	•
6.8 24.5 3.1392 5.4.3 5.	۲,	24.5	.11:	;	.251	31.3		31.9	3.2036	30.3	_
6.3 24.5 3.14655 0.94.4 6 6.9 24.5 6.9 3.1321 0.94.4 6 6.9 24.5 5.1321 0.94.4 6 6.9 25.6 6.9 3.1321 0.94.4 6 6.9 25.6 6.9 3.1321 0.94.4 6.9 25.6 6.9 3.1321 0.94.4 6.9 25.6 6.9 3.1321 0.94.9 6.9 25.6 6.9 3.132 0.94.9 6.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2.9 2	æ	24.5	.139	;	.228	31.1	35	51.2	•17	31.2	•
6.9 24.5 3.1922 54.5 54.5 6.9 5.1922 54.5 5.0 5.1922 55.6 5.0 5.0 1783 55.6 5.0 5.0 1783 55.6 5.0 17.0 256.3 5.0 17.0 256.3 5.0 17.0 256.3 5.0 17.0 256.3 5.0 17.0 256.3 5.0 17.0 256.3 5.0 17.0 256.3 5.0 17.0 256.3 5.0 17.0 256.3 5.0 17.0 256.4 5.0 256.4 5.0 256.4 5.0 256.4 5.	7 ;	24.5	.146	*	. 22	31.5	755	31.1	.17	31.1	۲,
69 25.6 3.1462 56.2 56.4 5 65.4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	£.	24.5	.132	•	.22	31.2	19	51.2	• 16	31.2	₹.
69 25.6 3.0163 56.9 56.9 56.9 56.9 56.9 56.0 3.0198 56.9 56.0 3.0198 56.9 56.9 56.1 2.0198 56.9 56.9 56.1 2.0198 56.9 56.1 2.0198 56.1 2.0	E.P	24.5	:::	*	•23	31.2	763	51.1	3.1800	31.1	3.4375
69 25.6 3.0198 56.4 57.1 67.1 7.0 26.1 2.0198 56.4 57.1 26.1 2.09778 65.0 1.0 26.1 2.09778 65.0 1.0 26.1 2.09778 65.0 1.0 26.1 2.09778 65.0 1.0 26.1 2.09778 65.0 1.0 26.4 2.09778 65.0 1.0 26.4 2.09778 65.0 1.0 26.4 2.09778 65.0 1.0 26.4 2.09778 65.0 1.0 26.4 2.09778 65.0 1.0 26.4 2.09778 65.0 1.0 26.4 2.09778 66.2 1.0 26.4 2.09778 66.2 1.0 26.4 1.0 26.	6-9	25.0	.078	ŝ	.14	31.4	٠7.	31.8	• 1 J	31.8	116
69 25.6 69 25.6 10 26.1 26.1 26.2 20 283 65.1 27 26.2 29 283 65.1 27 26.4 20 9378 65.1 27 26.4 20 9378 65.1 27 26.4 20 9378 68.7 27 26.4 20 9378 68.7 27 26.4 20 938 68.7 27 26.6 20 938 68.7 27 26.7 20 88.9 20 88.9 21 20 88.9 22 88.9 23 88.9 24 88.9 26 88.9 27 88.9 28 88.9 29 88.9 20 88.9	64	25.5	.013	•	=	31.7	1.7336	32.4	• 05	32.3	.925
67 25.9 2.9978 62.0 1 2 2 9 4 5 5 5 1 1 2 2 6 5 1 2 2 9 2 8 3 5 6 5 1 1 2 2 6 5 5 1 2 2 9 2 8 3 5 6 5 5 1 2 2 6 5 5 1 2 6 5 5 5 1 2 6 5 5	6.9	25.0	00.	-	-17	31.7	er,	37.6	۲.	32.5	912
70 26.3 2.9283 65.1 2 2 9283 7 65.1 2 2 9283 2 95.1 2 2 9283 2 95.1 2 95	63	25.5	76.	ď	.83	32.1	~	33.9	.91	33.7	304
70 26.3 2.9283 65.1 2 2 92.8 7 1 2 2 6.3 2 2 92.7 2 65.2 2 93.7 6 55.1 2 2 6.4 2 93.7 6 55.1 2 2 6.4 2 91.7 6 68.7 2 2 91.7 6 68.7 2 2 6.5 2 2 6.5 2 2 91.7 6 68.7 2 2 6.5 2 2 2 6.5 2 2 2 6.5 2 2 2 2 6.5 2 2 2 2 6.5 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	7.0	26.1	9	5	60.	31.7		34.8	A.	34.5	. 73?
7.1 26.3 2.9377 65.2 2.9377 7.1 26.4 2.9376 55.1 26.4 2.9376 55.1 26.4 2.9174 55.1 26.4 2.9174 57.4 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	76	26.5	92	ŝ	.694	31.7	1.7347	6.45	.83	34.5	131
71 26.2 2.9376 55.7 22.7 22.9376 55.7 22.94 2.9174 56.1 22.4 2.9174 57.4 22.9174 57.4 22.9174 57.4 22.9174 57.4 22.9174 57.4 22.9174 57.4 22.9174 57.4 22.9174 57.4 22.9174 57.1 22.9217 57.4 57.4 22.9217 57.4 27.7 57.4 27.7 57.4 27.7 57.4 57.4 57.4 57.4 57.4 57.4 57.4 5	7	ç	. 32	65.2	.6A9	31.9	1.7228	35.0	.82	34.5	127
71 26.9 2.9174 66.1 26.4 2.9174 66.1 26.4 2.9174 66.1 26.4 2.9174 66.7 2.9174 66.7 2.9174 66.7 2.9174 66.7 2.9174 66.7 2.9174 66.7 2.9174 66.7 2.9174 66.7 2.9174 66.2 2.9174 66.2 2.9174 66.2 2.9174 66.2 2.9174 66.2 2.9174 66.2 2.9174 66.2 2.9174 66.2 2.9174 66.2 2.9174 66.2 2.9174 66.2 2.9174 66.2 2.9174 66.2 2.9174 2.9174 66.2	7	÷	3	55.7	671	32.1	1.7137	ړ•٠٠٤	.82	34.7	. 123
71 26.4 2.9174 67.4 27.4 17.2 26.4 2.9158 68.7 68.7 26.4 2.9158 68.7 27.5 26.5 2.8897 67.5 26.5 2.8897 67.5 27.5 26.7 2.8897 67.5 27.5 27.5 2.8939 66.2 2.8939 27.5 27.5 2.8939 66.2 2.8939 27.5 2.8939 66.2 2.8939 27.5 28.9 27.5 2.8939 66.2 2.8939 27.5 2.8939	7.1	ç	95	46.1	4654	32.5	•	35.49	₹	34.7	. 221
71 26.4 2.9158 68.7 2 2 6.1 2 2 6.4 2 2 9 2 1 7 6 8 6 7 7 2 2 6 6 5 2 2 6 8 9 7 7 2 2 6 6 5 7 2 2 6 8 9 7 7 2 2 6 8 9 7 7 2 2 6 8 9 7 7 2 2 6 8 9 7 7 2 2 6 8 9 7 7 2 2 6 8 9 7 7 2 2 6 8 9 7 7 2 2 6 8 7 9 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	7.1	J	16.	57.4	5.00	32.4	1.6945	35.5	. 78	35.2	.5.R.A
71 26.4 2.9217 68.5 2 2 9138 68.7 2 2 66.5 2 2 9138 68.7 2 2 68.7 2 2 88.9 2 2 9138 68.7 2 2 68.9 2 2 68.9 2 2 68.9 3 66.2 2 2 68.9 3 2 69.3 66.2 2 2 68.9 3 2 2 89.9 3 66.2 2 2 88.9 3 2 2 88.9 3 66.2 2 2 88.9 3 66.2 2 2 88.9 3 66.2 2 2 88.9 3 66.2 2 2 88.9 3 66.2 2 2 88.9 3 66.2 2 8 89.9 3 66.2 3 2 8 8.9 3 66.2 3 2 8 8.9 3 66.2 3 2 8 8.9 3 66.2 3 2 8 8.9 3 6	7.1	٠Ç)	.91	68.7	.555	32.5	692	35.H	• 75	35.5	•65
72 26.6 2.8897 68.7 2.66.7 2.8897 65.9 67.5 2.6897 65.9 67.9 2.6897 65.9 2.6897 65.9 2.6897 65.9 2.6897 65.9 2.6897 65.9 2.6897 65.9 2.6897 65.9 2.6897 65.9 2.6897 65.9 2.8897 65.9 2.8897 65.9 2.8897 65.9 2.8897 67.1 2.8 2.8897 67.1 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8 2.8	1.1	£	.92	6.B.R	561	32.3	٦,	35.7	. 75	35.4	699
72 26.5 2.8897 67.5 2.8897 72 26.6 4.1 2.8857 65.9 65.9 2 2 68.9 3 65.9 65.9 2 2 68.9 3 66.2 2 68.9 3 66.2 2 68.9 3 66.2 2 68.9 3 66.2 2 68.9 3 66.2 2 68.9 3 66.2 2 68.9 3 66.2 2 68.9 3 66.2 2 68.9 3 66.2 2 68.9 3 66.2 3 67.9 3 66.2 3 67.9	7.2	ġ	.91	Ŧ	.554	37.5	σ	1.5 . H	• 75	35.5	.662
72 26.7 2.6862 63.9 2 2 13 26.7 2.8930 65.9 2 2 13 2 2 13 2 2 13 2 2 13 2 2 13 2 2 13 2 2 13 2 2 13 2 2 13 2 2 13 2 2 13 2 2 13 2 1	72	•	8.	~	.611	32.7	_	35.7	٠٦ن	35.4	.66₽
72 26.6 2.8930 65.6 2.8731 73 27.1 2.8731 66.2 2.8731 73 27.1 2.8733 66.2 2.8731 74 2.8731 2.8731 67.1 2.8731 74 2.8731 75 2.7531 75 2.7	12	4	88		147	32.7	1.682	6.4.	2.8314	54.7	2.7223
73 26.7 2.8791 64.1 2 7 1 3 27.1 2.8791 64.1 2 7 1 3 27.1 2.8791 66.2 7 1 3 2 2 8 3 9 7 66.2 7 1 3 2 8 9 9 7 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	12	÷	. 893	*	.758	32.5	683	X • 7 .	ď	્ય • 4 મ	23.5
73 27.1 2.8439 66.2 73 2.8197 67.1 73 28.9 2.8197 67.1 73 28.9 2.584 7 69.7 2 74.1 74.2 74.2 74.2 74.2 74.2 74.2 74.2 74.2	7.3	9	.873	,	.736	32.4	1.6829	15.0	.83	34.8	.714
73 27.3 2.8197 67.1 2 2 8 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6	7.3	-	8.	9	.652	12.9	1.6721	35.8	٠,۲	55.3	•
73 28.9 2.7549 67.4 2.954 7 32.7 2.3558 7 69.7 2 2 3558 7 78.9 2 2 3558 7 78.9 2 2 3558 7 78.9 2 2 3558 7 78.9 2 2 3558 7 78.9 37.1 2 2 3451 1 34995 3 34.8 1 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	73	~	. 31		116	32.3	1.6673	36.1	٠,۲	35.4	9
74 29.8 2.5847 (44.7 2.3558 7.8 78.9 7.8 78.9 7.8 78.9 7.8 78.9 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.8	7.3	Œ	. 75	۲.	663	33.1	1.6588	1.6.1	\$	36.4	a.
74 32.7 2.3558 78.9 2 2 3558 7 2 35.4 7	=	9	8	•	.51A	33.6	1.6360	3H . 7	ι. Ω	3A.1	2.4769
74 36.4 2.1174 89.4 17 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	=	CI	35	18.9	. 223	34.6	S.	ۍ د د	Ę.,	42.1	~
74 37.5 2.4461 33.1 1 1 1 2 2 3 3 3 1 1 1 1 2 3 3 3 3 3 3	7.	£	=	4. C.	. 961	35.6	1.5420	4H.2	٤	_	5
75 58.5 1.9995 97.1 75 59.5 1.94755 05.2 75 39.5 1.04755 04.5 76 41.5 1.0455 04.5 76 44.5 1.7455 04.5 76 44.1 1.7455 1.15.8 77 44.1 1.7475 1.15.8 77 44.1 1.7475 1.15.8	=	÷	-	1.3.5		36.6	1.05.	£ • c #	.91	œ	ς.
75 38.0 1.0700 06.2 1 1	7.5	÷	2	97.1	•	3.45	1.421	;• 1 ;	1.4197	5·1• t	•
75 39.5 1.99.6 95.4 17.5 17.5 17.5 17.5 17.5 17.5 17.5 17.5	15	æ	7.	0 f • 3			1.50%	٠	1.4151	50°1	•
75 39.6 1.59.8 3 34.8 1 1 2 3 3 3 4 3 4 3 4 3 4 3 4 3 4 3 4 3 4 3		ę,	4	4.36	1. 1796	\$f • ?	1.5156	٠1٠	1,7045	٠, ٠	• 476
76 41.5 1.9955 38.8 1. 76 41.5 1.8955 99.4 1. 76 40.1 1.786. 1.11.8 1. 77 44.1 1.7474 1.59 1. 77 46.4 1.664 1.11.8	1.,		•	3 4 9 4.	1.85.73	32.43	1.57276	¥•I:,	1.9339		خ
76 41-5 1-19555 99-4 1-7 1-7 1-7 1-7 1-7 1-7 1-7 1-7 1-7 1-7		<u>,</u>	•	34.0	1.775	¿•):	1.519.	•	I . D . 4	5.1.8	8.
76 40.1 1.7475 1.1.8 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7 1.7		-	•	999	~	54.44	1. 11 1	*)	1, -1, -1	52.	. 1 .
75 44.1 1.7475 1.3.2 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.		•	1.746.4	1,1,4	~	· • • • • • • • • • • • • • • • • • • •	1.56 ()	:	7 - 3 - 9		74.5
77 44.1 1.74'4 1.5.9 1. 77 45.4 1.6848 111.8 1.	1.	•	7.4		3. €/ • I		3	, • / • ,	7.7	5.	715
77 45.4 1.6644 111.6 1.5 77 45.5 1.665. 114.1 1.5	11	*				1.1.1	1.474	1.4.1	1.7428		₩.
77 46.5 1.6.5.0 114.1 1.	-	ď.	Ç	_	•	4.7.4	1.4.1.	•	•	57. 1	5 11
		c			1.5 1.5		1.46.1	, . .	1.66	54.	~;
0 T 0 C 1 T 0	1.1	2 = 13 4	. 43	_	7 11 14 14 T		-	- · ·	1.1 2	3.0	1.5014

HISTORICAL THELATION GUAFTERLY INDICES

							AGGPEGATE		AGGRE GATE	AIR VEHICLE
	AIRFRANE	FRUTUCTION	E 146 I NE	PRODUCT19h	AVIONICS	VIONICS PRODUCTION	EXCLUDING	AVIOUES	1401.30146	AVIONICS
	INDEX	FACTOR	INCEX	FACTOR	1:10F x	FACTOR	1.0£x	FACTOR	3 3CK 1	FACTOR
ر م د	160.0	F. 0.00.0	100.01	1.0:01	10.01	1.4000	1 000	1.0 2.39	140.1	1.3203
:				1	;		:			
7.8	47.5	1.6220	111.4	1.5751	39.4	1.3956	61.7	1.6032	4.65	1.5894
92	.B.1	1.5817	111.8	1.5535	39.7	1.3838	62.1	1.5762	5.5.4	1.5536
27	5°64	1.544.1	114.9	1. 5276	4.3.4	1.1721	6.9.3	1.5173	£19	1.5268
7.8	50.6	1.5230	114.8	1.5284	40.A	1.3467	6.47	1.5251	62.1	1.5135
7.3	51.1	1.4643	118.5	1.44.01	41.3	1 • 3303	66.5	1.4953	64.7	1.4762
19	55.0	1.39 16	127.9	1.3722	42.0	1.3070	711.2	1.3886	68.3	1.5836
79	56.4	1.3653	1.54 . 5	1.3049	43.4	1.2668	73.7	1.3409	7.07	1.3364
61	59.2	1.3011	158.2	1.1089	***	1.2375	A1.7	1.2178	77.5	1.2191
. 8	62.2	1.2386	179.4	C.9782	47.0	1.1637	33.2	1.1219	84.1	1.1235
90	17 4 9	1.1941	168.9	1.0391	48.9	1.1235	R7.7	1.1278	85.9	1.1275
8	65.3	1.1795	169.1	1.0379	50.3	1.0927	88.3	1.1193	84.5	1.1177
¢	66.8	1.1534	156.7	1.0529	50.8	1.0819	4.9.0	1.1115	85.1	1.1098
14	71.2	1.0815	179.1	1.1315	51.9	1.0583	93.2	1.0612	89.1	1.161.
81	14.€	1.0294	112.9	1.0148	52.4	1.0467	36.6	1.0235	92.2	1.0253
8	76.5	1.0070	174.5	1.0.58	53.7	1.0229	98.2	1.0455	93.8	1.0675
8	77.2	0.9972	174.4	1.0061	53.8	1.020%	9.4.6	1.0007	1.046	1.0012
2	77.0	C. 9841	175.1	1.0021	55.1	6.9964	34.5	0.9935	95.1	0.9937
۵2	76.4	1.2001	174.6	9.16.U	55 3	0.39.5P	0.3.0	0.4385	94.0	11.9943
6	16.0	1.0141	175.1	Catte C. O	55	1.16.0	2.48€	1.0.175	93.9	1.1063

HISTORICAL INFLATION FISCAL YEAR INDICES

	AIRFRAME	AIRFRAME PRODUCTION	EWEINE	PRODUCTION	SOINGIAV	AVISHICS FRODUCTION	AGSPEGATE Excluding	AIR VEHICLE Avionics	AGGREGATE Including	AIR VEHICLE Avionies
	1 JON1	FACTOR	17.DEX	FACTOR	1 40F X	FACTOR	1.10E x	FACTOR	I NOE K	FACTOR
,	100.0	F Y R Z =	154.4	1.03.4	1010	1 4 8 2 8	1545.	1.0301	101.0	1,0040
: :		;				;				
6 '	24.3	3.1644	93.8₽	3.2624	31.3	1 - 7554	59.3	3.2129	\$1.9	1.1564
53	54.9	3.4922	55.2	3.179º	31.4	1.7536	11.6	3,1261	31.6	2.9895
7.0	56.1	2.9631	62.3	2,9153	31.9	1.7293	34.1	2.9039	35.3	2.1028
7.1	26.2	2.9341	66.1	2.6542	32.2	1.7948	55.1	2.4170	34.5	2.7140
72	26.5	2.91:2	68.3	2.5674	32.5	1.6914	35.8	2.7545	35.4	2.5563
73	3.65	2.8759	4.44	2.7230	32.7	1.4816	\$5.1	2.8136	34.3	2.1076
:	59.4	2.6155	7.3.H	2.4799	33.5	1.6373	34.6	2.5533	38.1	204790
75	31.5	2.0332	93.9	1.8679	36.4	1,5141	54.3	1.9445	48.3	1.9308
7.E	40.8 43.1	1.9135	97.0	1.8096	36.2 36.6	1.5183	0 C C C C C C C C C C C C C C C C C C C	1.8712	51.2 54.2	1.8462
11	0.484	1.7117	149.0	1.6167	37.3	1.4733	59.7	1.6741	57.1	1.6572
7.4	48.1	1.5993	112.8	1.5554	39.3	1.5365	ۍ د د	1.5917	61.2	1.0593
70	53.4	1.4416	123.9	1.4151	6.14	1.3120	63.1	1.4314	4.99	1.4239
£.	62.8	2266	168.9	1.1390	47.6	1,1533	3.5 . 4	1.1451	82.5	1.1455
ī	72.2	6+90-1	171.0	1.1259	52.2	1.4525	44.2	1.9492	e • 66	1.0494
~ .	77.	0 - 00 - T	175.5	1.3000	54.9	1.4904	6*86	1.0000	94.5	1.0949

